

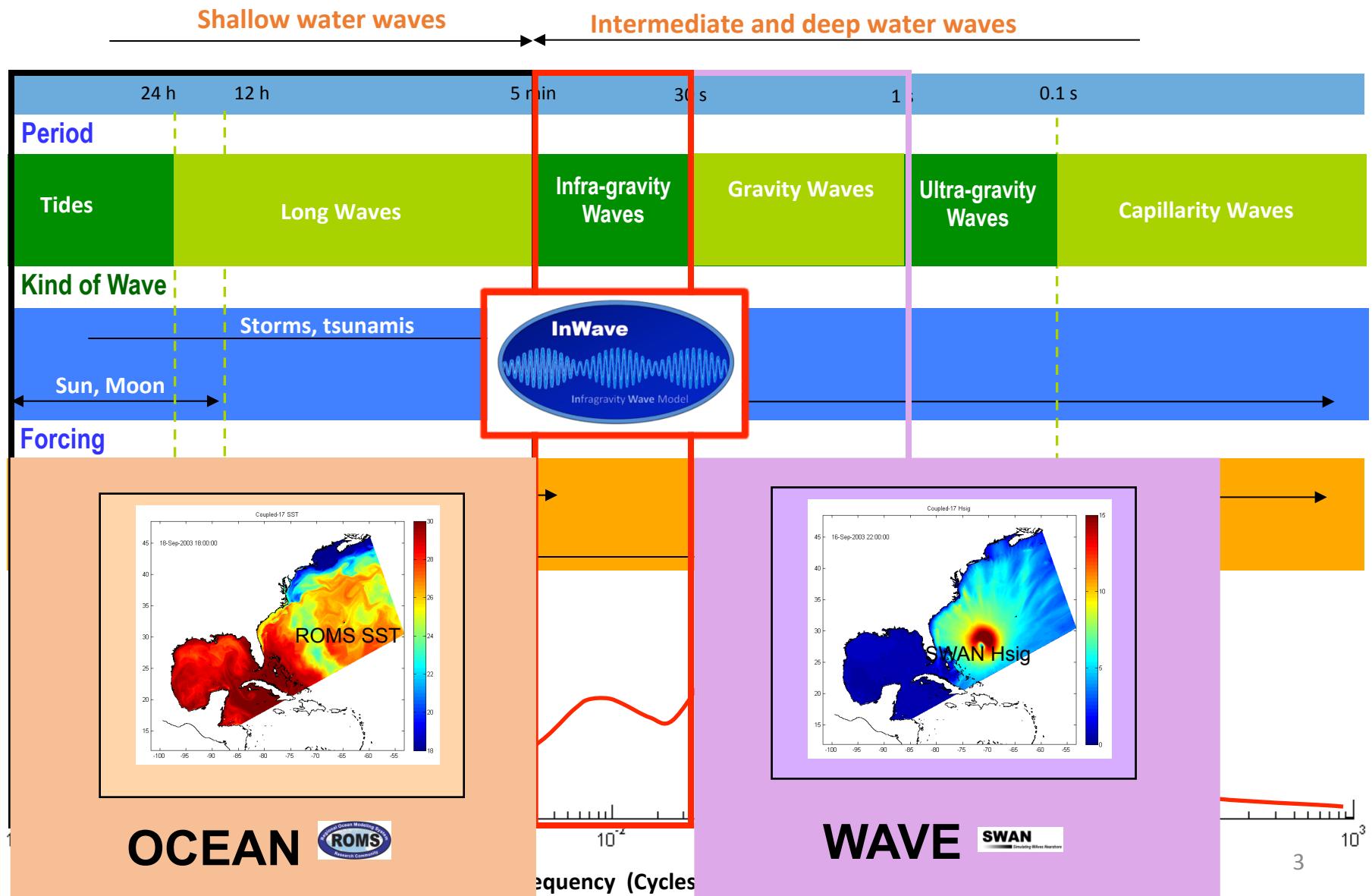
INWAVE: THE INFRAGRAVITY WAVE DRIVER OF COAWST

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John C. Warner**

**COAWST WORKSHOP
Woods Hole, 15th -19th August, 2016**

OUTLINE

1. INTRODUCTION AND MOTIVATION
2. IG WAVE GENERATION AND DISSIPATION MECHANISMS
3. IG WAVE MODELLING TECHNIQUES
4. INWAVE
 - a. EQUATIONS AND NUMERICAL SCHEME
 - b. HOW IS IT LINKED TO THE VORTEX FORCE?
 - c. APPLICATIONS
 - d. FUTURE PLANS



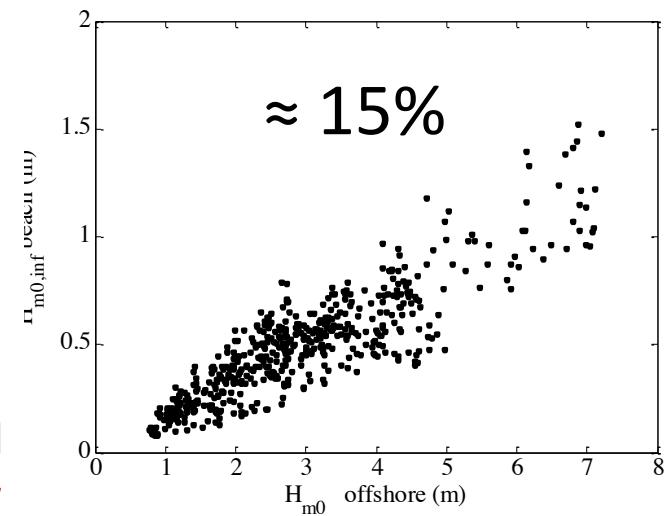
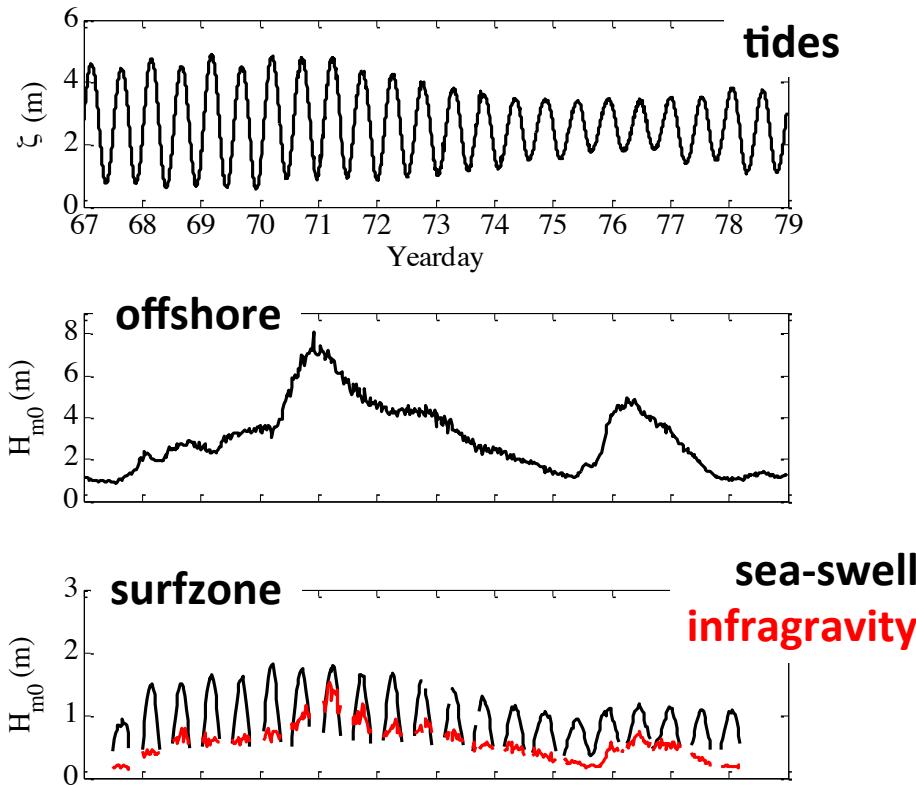
- InfraGravity (IG) waves are defined as waves with **periods between 30 and 300 seconds** generated by the **non-linear interactions of gravity waves**.
- In deep water the energy transfer to IG waves is non-resonant and the height of the IG waves is few millimeters. In **shallow water** the **energy transfer becomes near-resonant** and IG wave height can increase to over 1 m.
- IG waves are highly correlated with the modulation of wind or swell waves.

RUNUP AND BEACH-DUNE EROSION

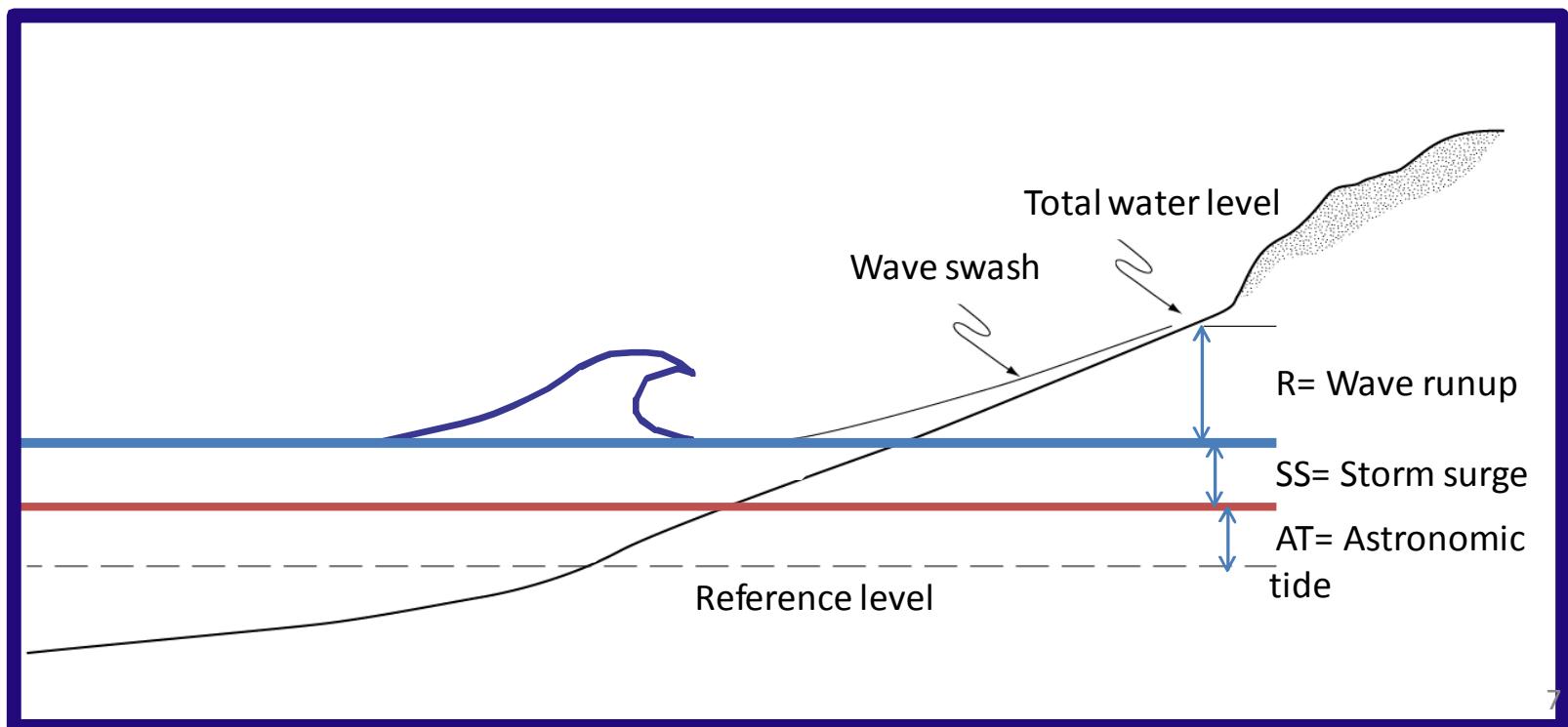
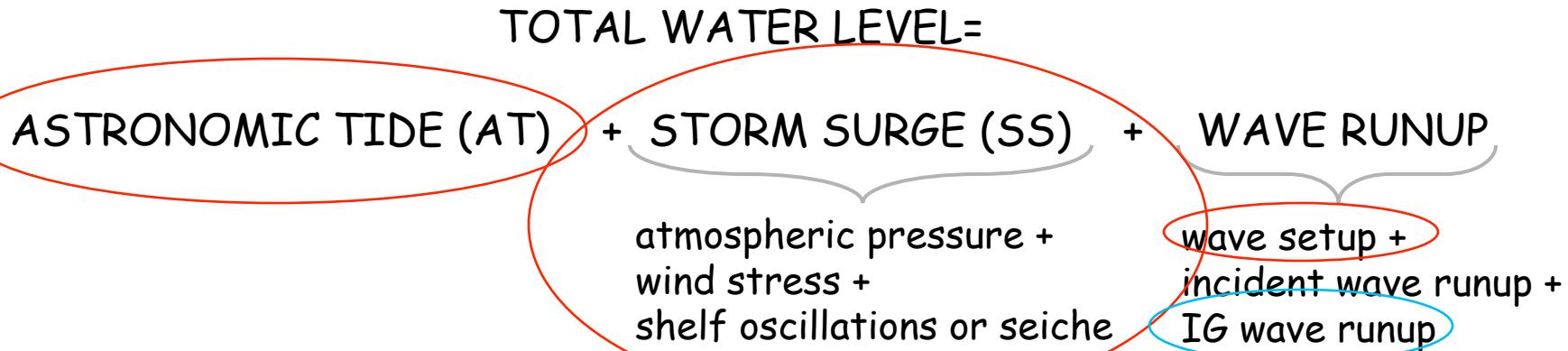


HARBOR RESONANCE



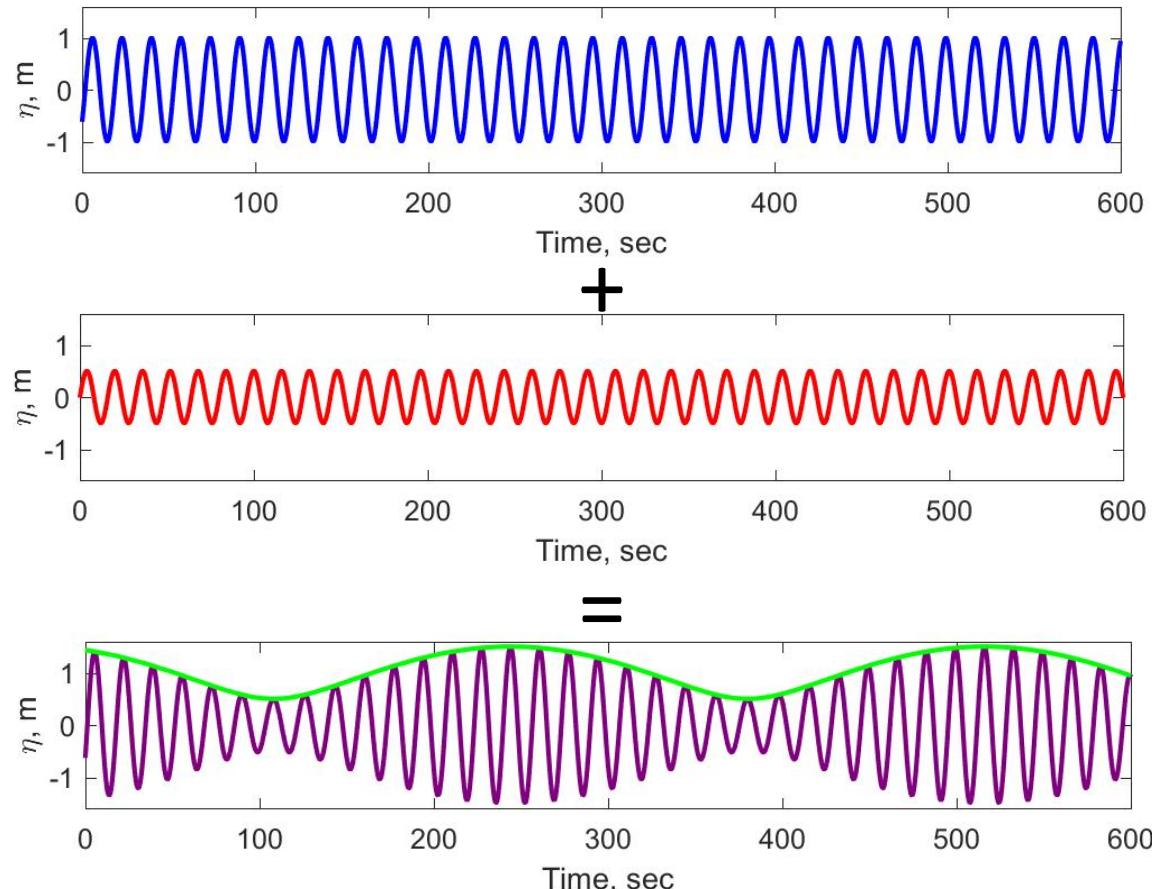


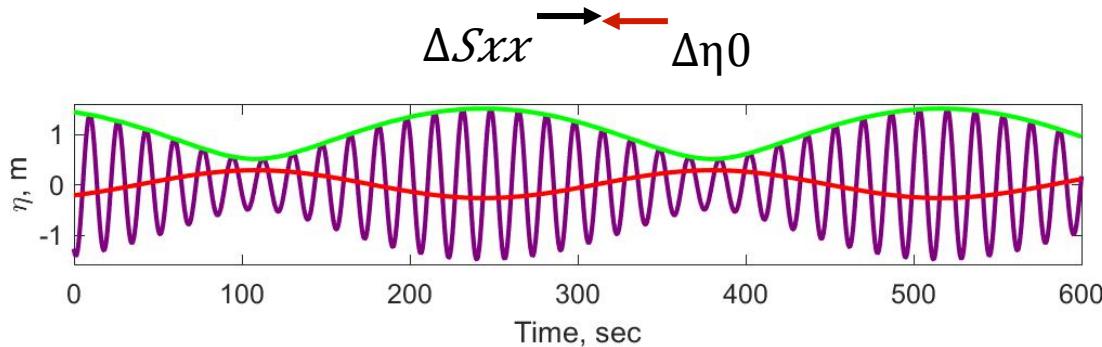
Ruessink, B.G. (2010). Observations of turbulence within a natural surf zone. *Journal of physical oceanography*, 40 (12).



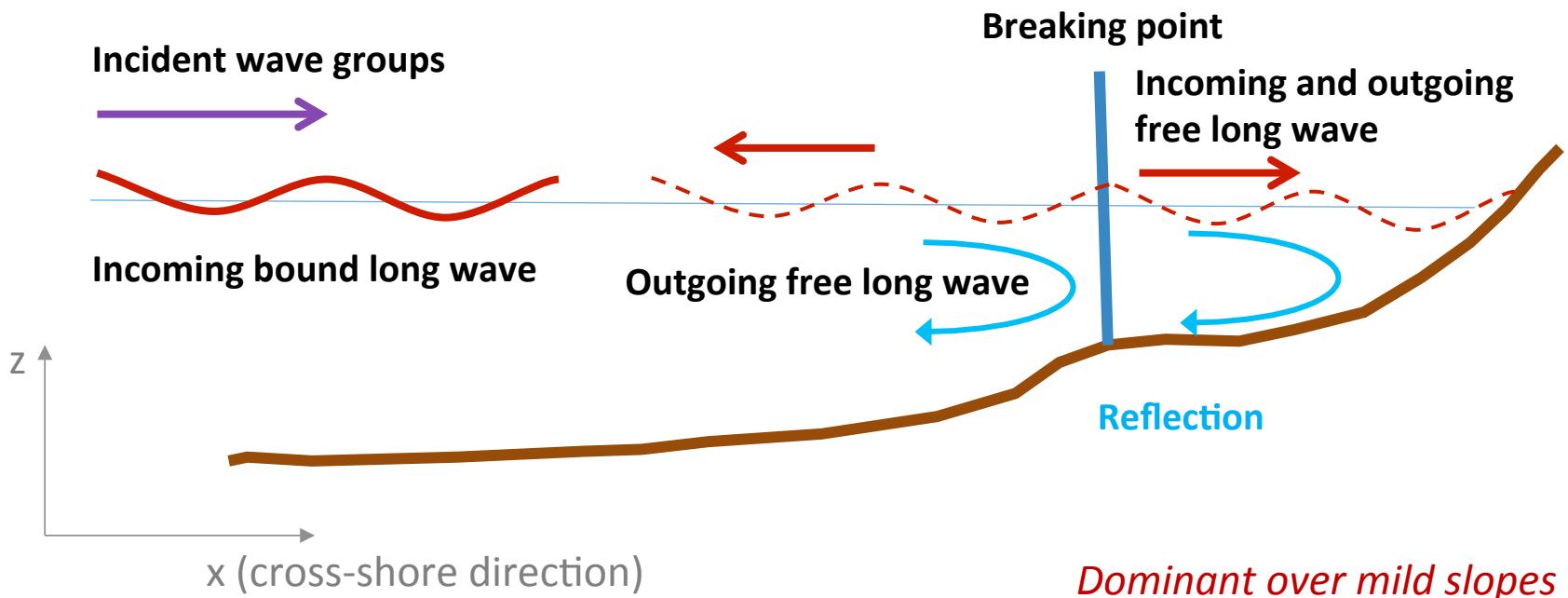
GENERATION MECHANISMS

1. GROUP-BOUND WAVE GENERATION AND SHOALING: Quadratic difference interaction among pairs of primary waves, resulting in group-bound second-order waves (Biesel, 1952; Longuet-Higgins and Stewart, 1962).



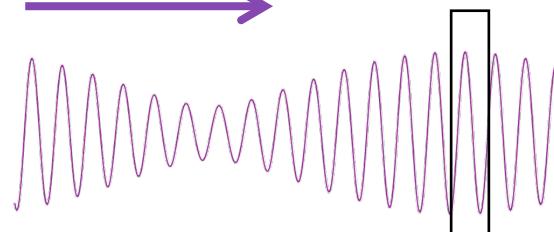


η_0 = wind-wave
averaged
water level
 S_{xx} = radiation stress

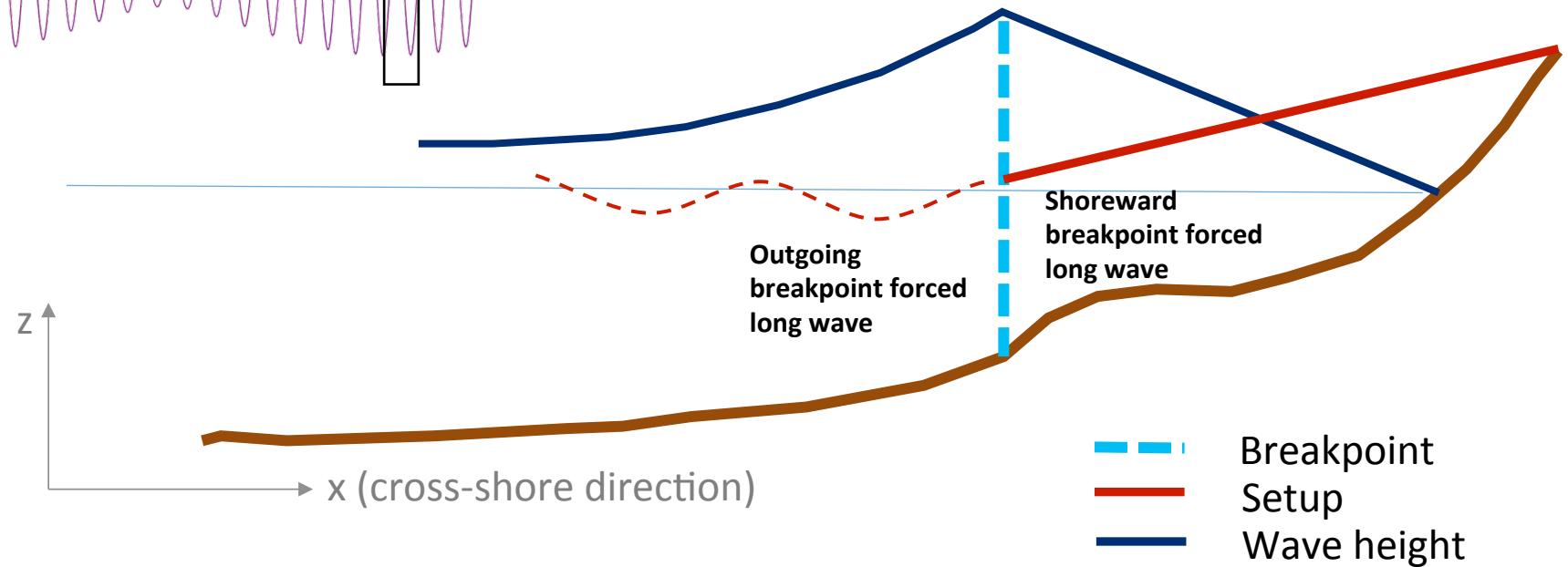


2. BREAK-POINT MOVEMENT: Symonds et al., 1982; Symonds and Bowen, 1984, Schaffer and Jonsson, 1990 and Schaffer, 1990.

Incident wave groups



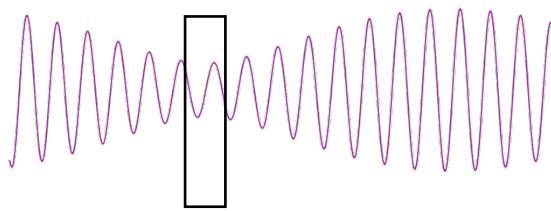
Breaking point variation



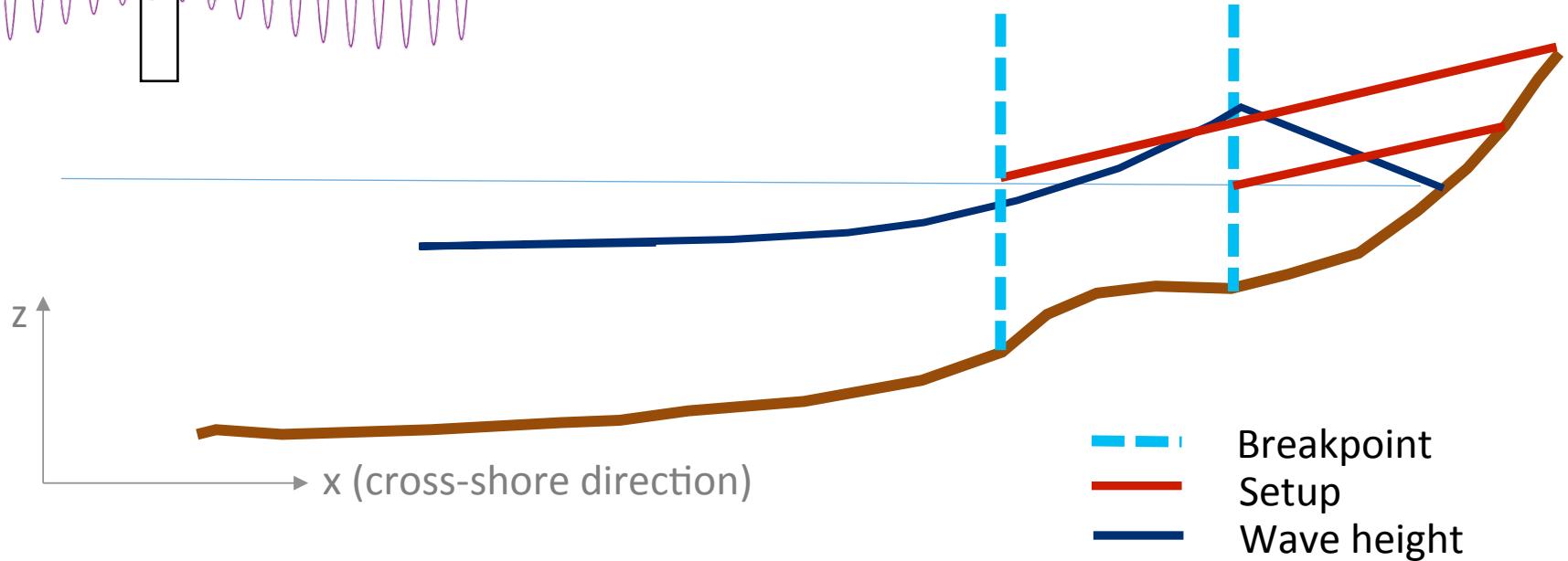
Dominant over steep slopes

The highest waves in the wave group produce a higher setup than the smallest waves: wave group modulation of the wave setup

Incident wave groups



Breaking point variation



GENERATION MECHANISMS

*Battjes, J. A., H. J. Bakkenes, T. T. Janssen, and A. R. van Dongeren (2004),
Shoaling of subharmonic gravity waves, J. Geophys. Res., 109, C02009.*

$$\beta = \frac{h_x \sqrt{gh}}{w} \quad \beta = \text{Normalized bed slope}$$

h_x = bed-slope

w = long-wave frequency (rad s^{-1})

h = water depth (m)

Breakpoint mechanism is dominant over steep slopes $\beta > 1$

Bound-wave shoaling is dominant over mild-slopes $\beta \leq 0.3$

DISSIPATION MECHANISMS

- Bottom friction (Henderson and Bowen, 2002; de Bakker et al., 2014).
- Non-linear energy transfer back to sea-swell frequencies through triad interaction (Henderson et al., 2006; Thomson et al., 2006; Guedes et al., 2013).
- IG wave breaking (Battjes et al., 2004; Van Dongeren et al., 2007; Lin and Hwung, 2012; Nazaka and Hino, 1991).
- Energy transfer thru non-linear interactions to lower periods.

It is not clear which is the main dissipation mechanism and it might depend on the beach slope and on the frequency of the IG components.

MODELLING APPROACHES OR TECHNIQUES

WAVE RESOLVING TECHNIQUES:
BOUSSINESQ , PARTICLE METHODS, NON-HYDROSTATIC MODELS OR RANS MODELS

WAVE AVERAGED OR PHASE AVERAGED
TECHNIQUES:
WAVE ACTION BALANCE EQUATION + NLSW

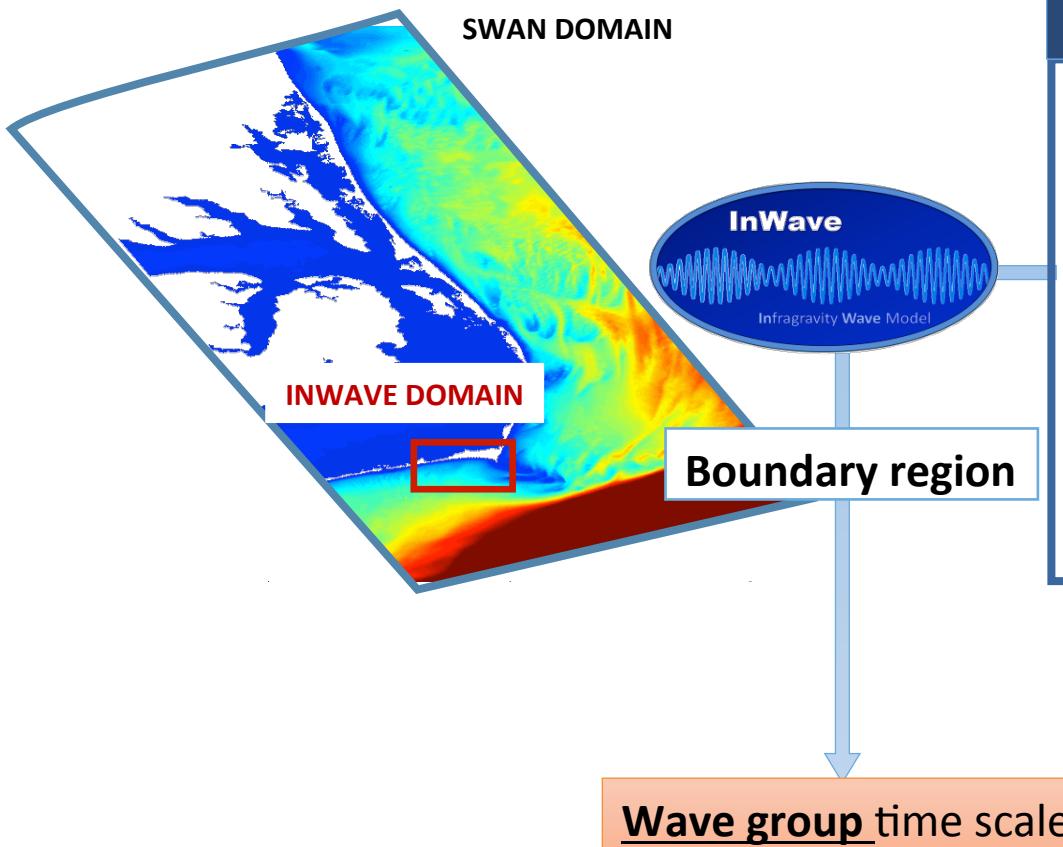
Modeling approaches: from Reniers, 2012 (Long Wave and Runup Workshop)

Dimension	Short wave resolving	Short wave averaged	LSWE	NSWE	RANS	NH	BSNQ	WKB
1D	2,7,8	1,30,3,5,9	1,5,9	2,30,3			7,8	
1D+		10,11,25, 26	10,11,26					25
2DH	18,17, 32	15,14,23		15,14,23			18,17,3 2	
2DV	33				33			
Q3D		30		30				
3D	22	19		19		22		

[1] List [1992], [2] Watson and Peregrine [1992], [3] Roelvink [1993], [4] Karunarathna and Tanimoto [1995], [5] Symonds et al. [1982], [6] Van Leeuwen [1992], [7] Bosboom et al. [], [8] Rhaka et al. [1997], [9,10] Shaffer [1993,1994], [11] Reniers et al. [2002], [12] MacMahon et al., [2010], [13] Herbers and Burton [1997], [14] Van Dongeren et al. [2003], [15] Long and Ozkan-Haller [2009], [16] Chen and Guza [1993], [17] Chen et al., [2003], [18] Spydell and Feddersen [2009]. [19], Reniers et al., [2009], [20] Uchiyama et al. [2010], [21] Janssen et al. [2009], [22] Stelling and Zijlema [2010], [23] Roelvink et al. [2009], [24] Foda, M. A., and C. C. Mei [1981], [25] Herbers et al. [1995], [26] Howd et al. [1992], [27] Lippmann et al. [1997], [28] Madsen et al., [1997], [29] Henderson et al. [2006], [30] Van Dongeren and Svendsen [2000], [31] Haller et al. [1999], [32] Johnson and Pattiaratchi [2006], [33] Bakhtyar et al. [2009], [34] Thompson et al. [2007], etc.

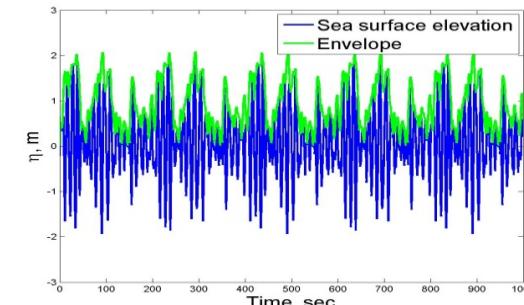
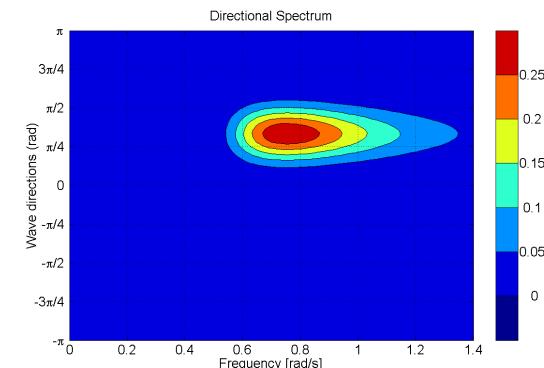
INWAVE IS BASED ON THE WAVE AVERAGED OR PHASE AVERAGED TECHNIQUE

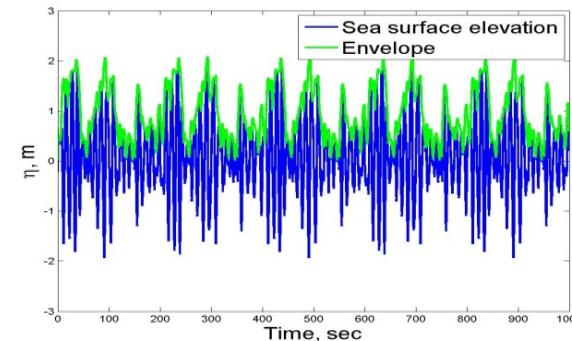
INWAVE IS SIMILAR TO XBEACH MODEL (Roelvink et al., 2009) BUT WITH THE DIFFERENCE THAT INWAVE+ROMS IS ABLE TO SIMULATE **3D CIRCULATION** WHILE XBEACH IS 2D



SWAN domain: Wave spectral time scale

DIRECTIONAL WAVE SPECTRUM





FREE SURFACE ELEVATION AND WAVE ENERGY ENVELOPE TIME VARIATION



Boundary condition for the wave action conservation equation

$\partial A/\partial t + \partial c \downarrow g_x A/\partial x + \partial c \downarrow g_y A/\partial y + \partial c \downarrow g_\theta A/\partial \theta = -D/\sigma$ where $A(x,y,\theta,t)=E(x,y,\theta,t)$
wave energy/ $\sigma(x,y,t)$ *intrinsic frequency*



Vortex Force terms varying
in wave group scale

Wave group scale varying
Wave forcing



Infragravity wave generation +
3D hydrodynamics

MAIN MODULES OF INWAVE

READ SWAN DIRECTIONAL
SPECTRAL OUTPUTS AT
THE CHILD GRID BOUNDARIES

RECONSTRUCT THE GROUP SCALE
VARYING WAVE ACTION TIME SERIES
AT THE CHILD GRID BOUNDARY

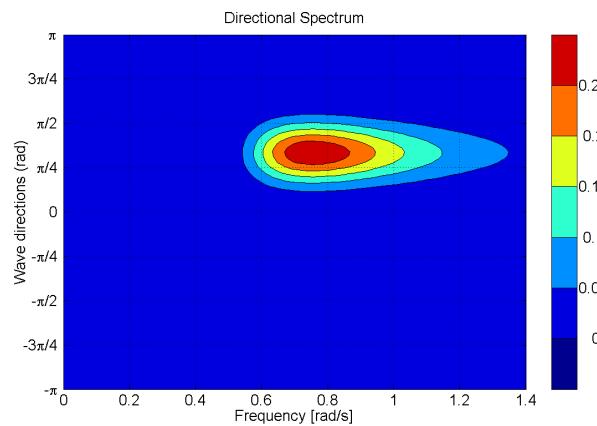
RECONSTRUCT THE INCOMING
BOUND INFRAGRAVITY WAVES
(e.g. Herbers et al. 1994)

PROPAGATE IN TIME AND SPACE
THE GROUP VARYING WAVE
ENERGY AT THE CHILD GRID

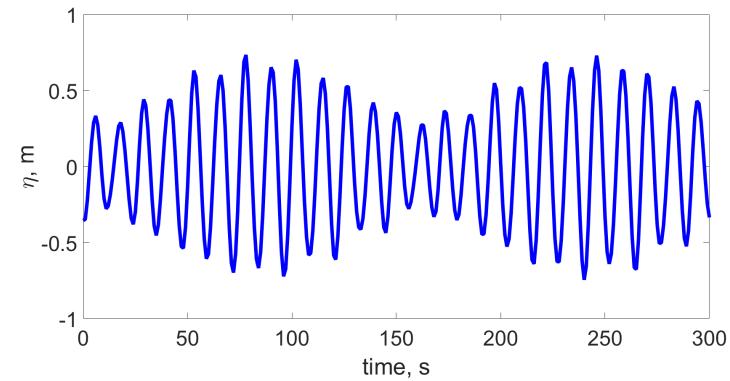
USE THE GROUP VARYING WAVE ENERGY FORCING AS INPUTS
FOR THE VORTEX-FORCE (VF) IN ROMS

Infragravity wave generation thru VF and propagation of
the bound IG wave **ROMS**

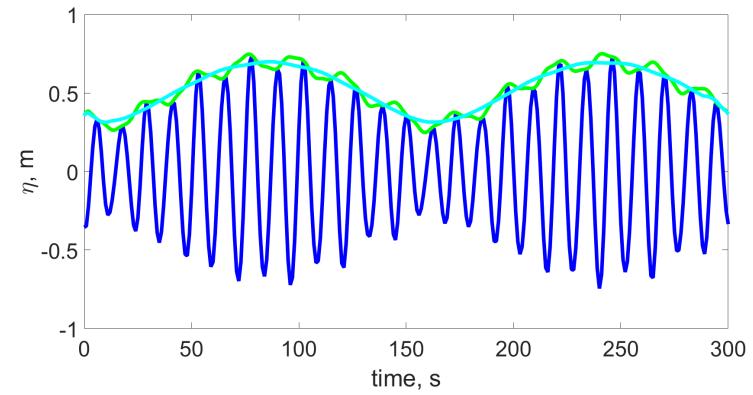
Leaky, bound and trapped infragravity waves



RANDOM PHASES +
INVERSE FFT



HILBERT TRANSFORM +
LOW-PASS FILTER



$$A(x, y, \theta, t) = \frac{E(x, y, \theta, t)}{\sigma(x, y, t)} = \frac{1}{2} \rho g |A_{low}(x, y, \theta, t)|^2$$

at INWAVE boundaries

For each realization $A(x, y, \theta, t)$ is going to be different

RECONSTRUCT THE INCOMING BOUND INFRAGRAVITY WAVES

Van Dongeren et al. (2003) -> Hasselman (1963) & Herbers et al. (1994)

1. The energy of the secondary forced elevation $E_3(\Delta f)$ for one particular pair of interacting primary waves can be computed following Herbers et al. (1994)

$$E_3(\Delta f) = 2 \int_{\Delta f}^{\infty} \int_0^{2\pi} \int_0^{2\pi} D^2(f + \Delta f, -f, \Delta\theta + \pi) \cdot E(f + \Delta f, \theta_1) E(f, \theta_2) d\theta_2 d\theta_1 df,$$

$$\begin{aligned} D(-f_1, f_2, \Delta\theta + \pi) &= f_2 = f_1 + \Delta f. \\ &\equiv \frac{g k_1 k_2 \cos(\Delta\theta + \pi)}{8\pi^2 f_1 f_2} \frac{\cosh(k_3 h)}{\cosh(k_1 h) \cosh(k_2 h)} \\ &- \frac{g(-f_1 + f_2)}{\left[g k_3 \tanh(k_3 h) - (2\pi)^2 (-f_1 + f_2)^2 \right] f_1 f_2} \\ &\times \left\{ (-f_1 + f_2) \left[\frac{(2\pi)^4 (f_1 f_2)^2}{g^2} - k_1 k_2 \cos(\Delta\theta + \pi) \right] \right. \\ &\left. - \frac{1}{2} \left[\frac{-f_1 k_2^2}{\cosh^2(k_2 h)} + \frac{f_2 k_1^2}{\cosh^2(k_1 h)} \right] \right\}, \end{aligned}$$

$$k_3 \equiv |\vec{k}_1 - \vec{k}_2| = \sqrt{k_1^2 + k_2^2 - 2 k_1 k_2 \cos(\Delta\theta)}.$$

$$A_3 = \sqrt{2 E_3 df},$$

2. Bound wave out of phase with the envelope formed by each interacting pair

$$\psi_3 = \psi_2 - \psi_1 + \pi.$$

3. The direction of the bound wave is given by

$$\theta_3 = \arctan \left(\frac{k_2 \sin \theta_2 - k_1 \sin \theta_1}{k_2 \cos \theta_2 - k_1 \cos \theta_1} \right).$$

4. The time series of the surface elevation of the bound wave is

$$\tilde{\zeta}_3(0, y, t) = A_3 \cos(k_3 \sin \theta_3 y - 2\pi \Delta f t + \psi_3).$$

5. This process is repeated for every pair of short-wave components. The summation of all components gives the total bound wave.

Wave action balance equation in Cartesian coordinate system

$$\partial(A)/\partial t + \partial(C \downarrow g, x A)/\partial x + \partial(C \downarrow g, y A)/\partial y + \partial(C \downarrow g, \theta A)/\partial \theta = -D \downarrow w / \sigma$$

$$C \downarrow g, x = C \downarrow g \cos \theta + U$$

$$C \downarrow g, y = C \downarrow g \sin \theta + V$$

Wave dispersion relation + Doppler relation

$$\sigma = \sqrt{gk} \tanh(kh)$$

$$C \downarrow g = 0.5 C (1 + 2kh / \sinh(2kh))$$

$$C = gk \tanh(kh) / \sinh(2kh)$$

$$w = \sigma + k \cdot u$$

Eikonal equation

$$\partial k \downarrow x / \partial t = -\partial(w) / \partial x$$

$$\partial k \downarrow y / \partial t = -\partial(w) / \partial y$$

$$|k| = k \downarrow x \gamma 2 + k \downarrow y \gamma 2$$

Wave breaking

$$D\downarrow w = D\downarrow b \cdot Q\downarrow b$$

$D\downarrow w$ =Total energy dissipation

$D\downarrow b$ =Energy dissipation in a breaking wave

$Q\downarrow b$ =Fraction of breaking waves

Roelvink (1993)

$$Q\downarrow b = \min(1, 1 - \exp(-(H/\gamma h)^{\uparrow n}))$$

$$H = \gamma h$$

γ =Breaking parameter

h =water depth

H =wave height

Battjes and Janssen (1978)

$$D\downarrow b = 2\alpha f\downarrow rep E\downarrow w$$

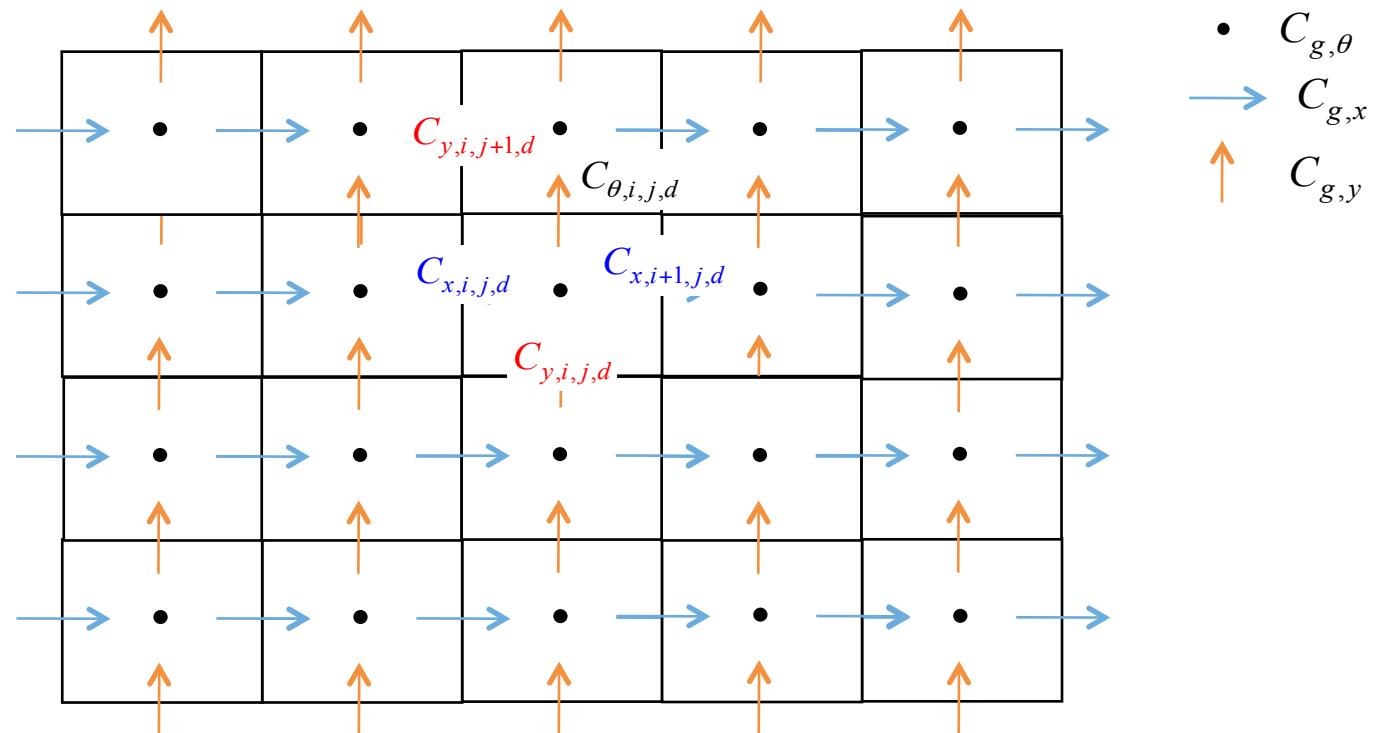
α =Coefficient $O(1)$

$f\downarrow rep$ =Representative frequency

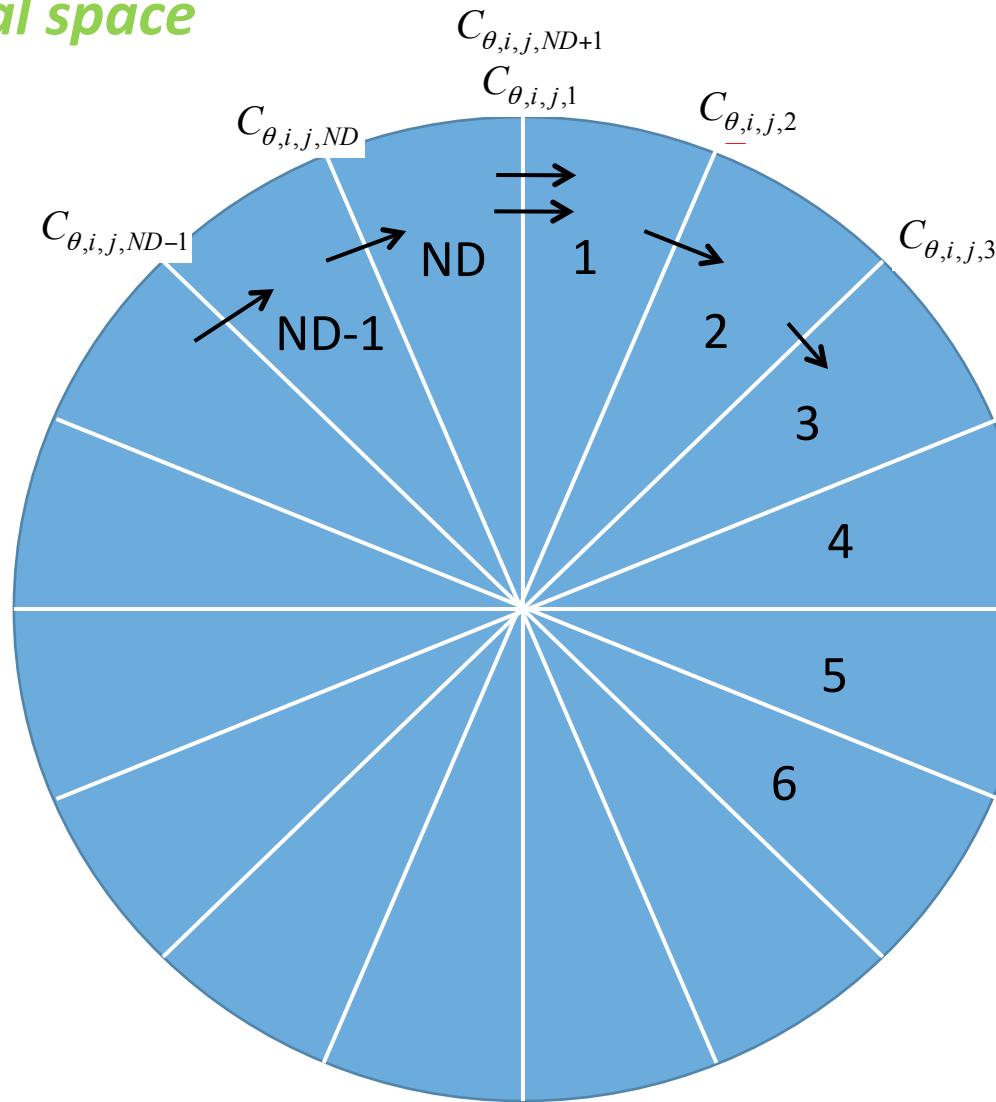
$E\downarrow w$ =Wave energy integrated over directions

n =Coefficient

Horizontal space



Directional space





/* Master list of all InWave cpp options

```
*# define INWAVE_MODEL      use to turn ON or OFF InWave model
*# define INWAVE_SWAN_COUPLING    use to turn ON or OFF InWave SWAN coupling
*# define DOPPLER          use to turn ON or OFF the effect of currents on the dispersion relation
*# define ACX_ADVECTION     use to turn ON or OFF advection of Ac in the xi direction
*# define ACY_ADVECTION     use to turn ON or OFF advection of Ac in the etai direction
*# define ACT_ADVECTION     use to turn ON or OFF advection of Ac in the directional direction
*# define ENERGY DISSIPATION use to turn ON or OFF energy dissipation
*# define ROELVINK         use to turn ON or OFF Roelvink energy dissipation
```

******* AC IN X-Y SPACE *******

*# undef WEST_AC_CLAMPED	Western edge, clamped condition for Ac
*# undef WEST_AC_GRADIENT	Western edge, gradient condition for Ac
*# undef WEST_AC_RADIATION	Western edge, radiation condition for Ac
*# undef WEST_AC_WALL	Western edge, wall condition for Ac

*# undef EAST_AC_CLAMPED	Eastern edge, clamped condition for Ac
*# undef EAST_AC_GRADIENT	Eastern edge, gradient condition for Ac
*# undef EAST_AC_RADIATION	Eastern edge, radiation condition for Ac
*# undef EAST_AC_WALL	Eastern edge, wall condition for Ac

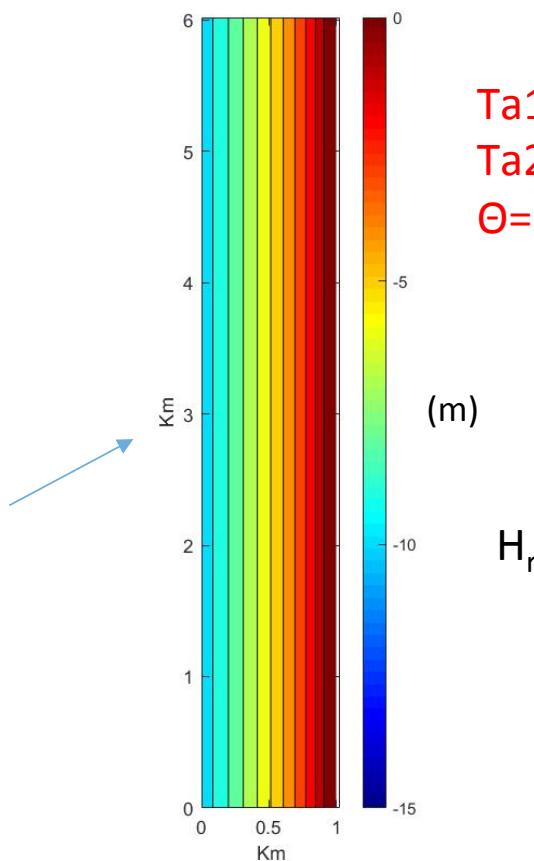
*# undef NORTH_AC_CLAMPED	Northern edge, clamped condition for Ac
*# undef NORTH_AC_GRADIENT	Northern edge, gradient condition for Ac
*# undef NORTH_AC_RADIATION	Northern edge, radiation condition for Ac
*# undef NORTH_AC_WALL	Northern edge, wall condition for Ac

3D CASE IDEALIZED APPLICATION: OBLIQUE INCIDENT BICHROMATIC WAVES



Matlab files for test cases inputs: `create_Inwave_files.m`

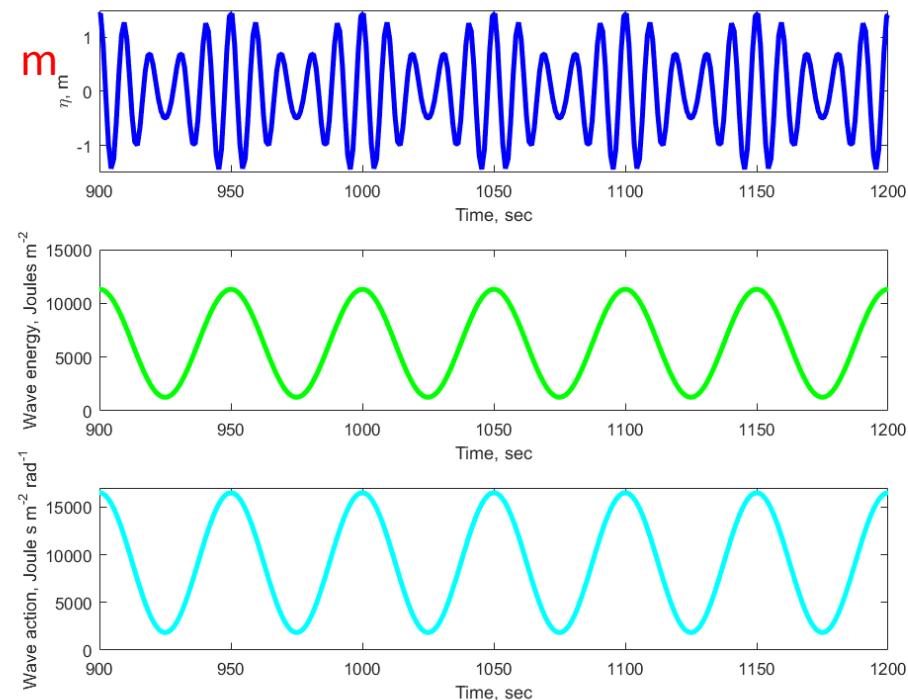
`create_Inwave_grd.m`



`create_Inwave_ini.m`

$Ta1=10 \text{ s}, a1= 1 \text{ m}$
 $Ta2= 8.3 \text{ s}, a2=0.5 \text{ m}$
 $\Theta= 261 \text{ degrees}$

`create_Inwave_bnd.m`



CCP OPTIONS

```
#define ROMS_MODEL
#define INWAVE_MODEL

#define ACX_ADVECTION
#define ACY_ADVECTION
#define ACT_ADVECTION
#undef DOPPLER

#define WEC_VF
#define ENERGY_DISSIPATION
#define WDISS_INWAVE
#undef ROELVINK
```

```
! Number of grid nesting layers. This parameter is used to allow refinement
! and composite grid combinations.

NestLayers = 1

! Number of grids in each nesting layer [1:NestLayers].

GridsInLayer = 1

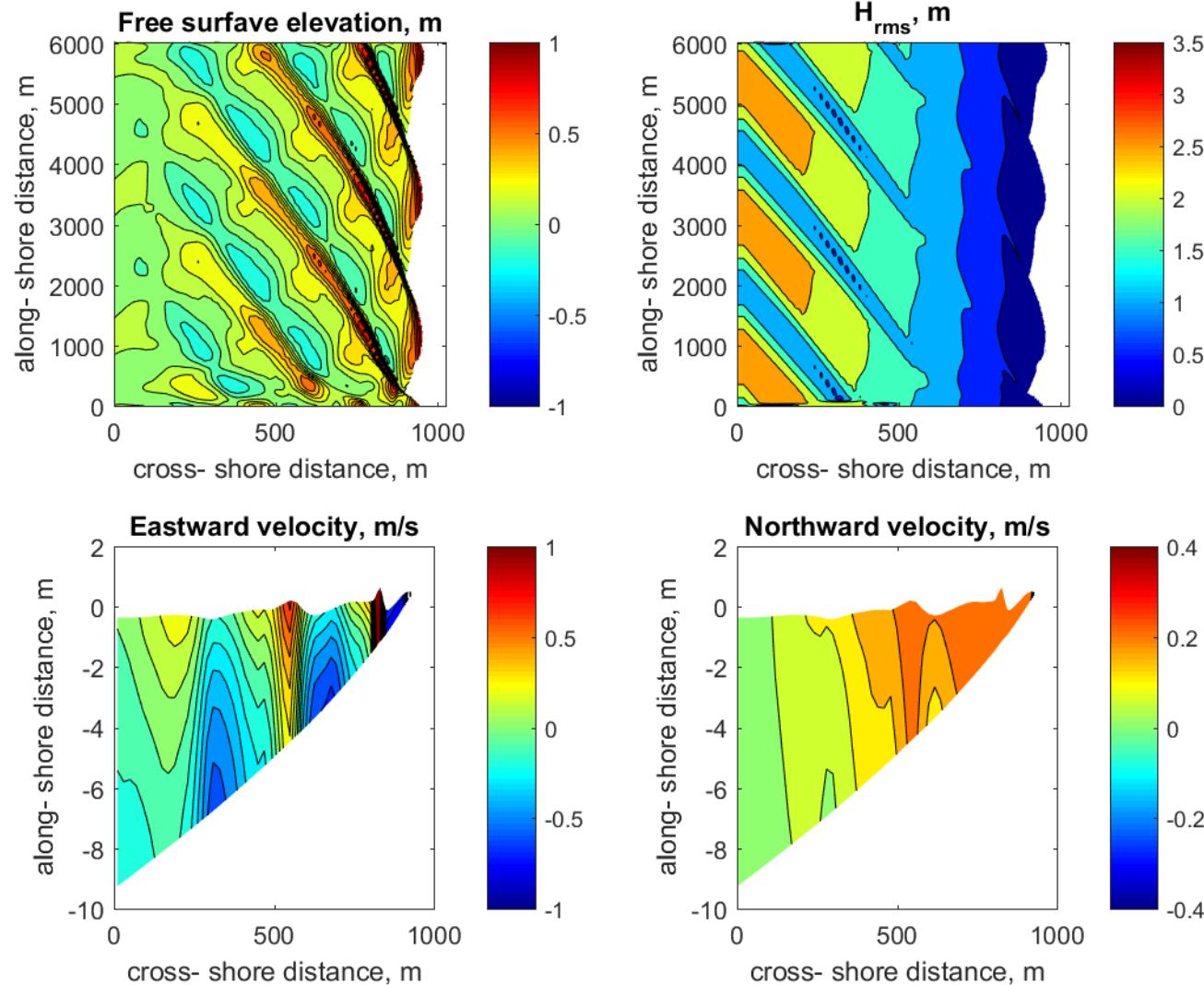
! Grid dimension parameters. See notes below in the Glossary for how to set
! these parameters correctly.

Lm == 120           ! Number of I-direction INTERIOR RHO-points
Mm == 300           ! Number of J-direction INTERIOR RHO-points
N == 11             ! Number of vertical levels
ND == 11            ! Number of wave directional bins

Nbed = 1            ! Number of sediment bed layers

NAT = 2             ! Number of active tracers (usually, 2)
NPT = 0             ! Number of inactive passive tracers
NCS = 0             ! Number of cohesive (mud) sediment tracers
NNS = 1             ! Number of non-cohesive (sand) sediment tracers
```

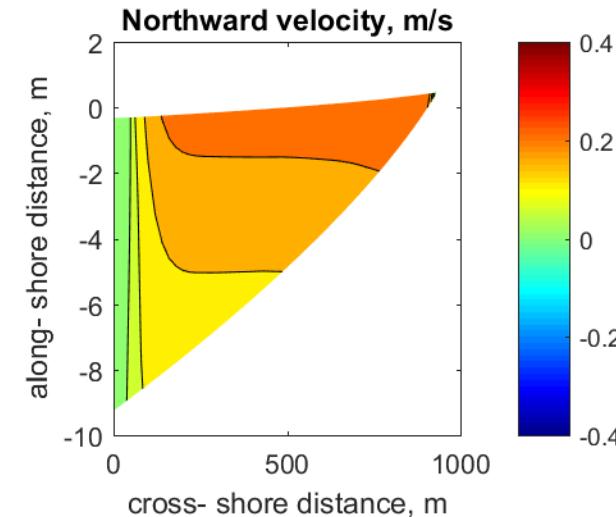
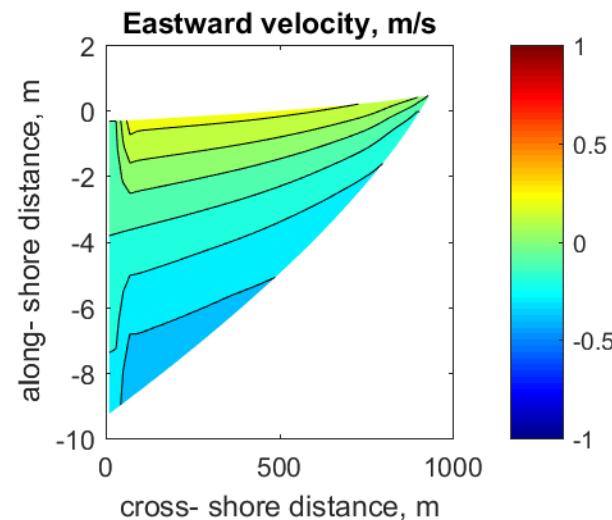
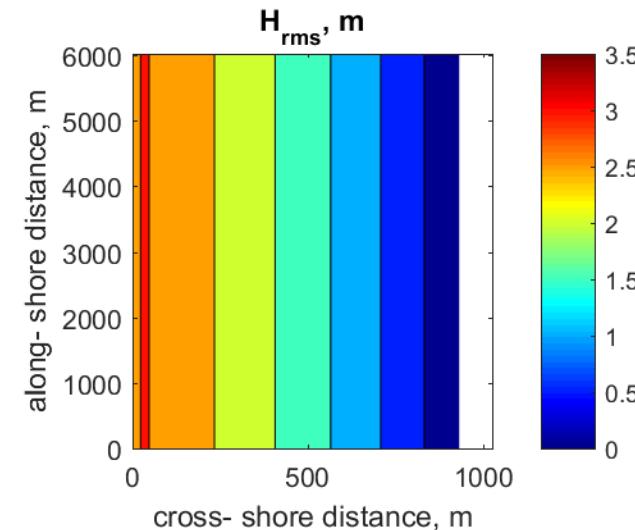
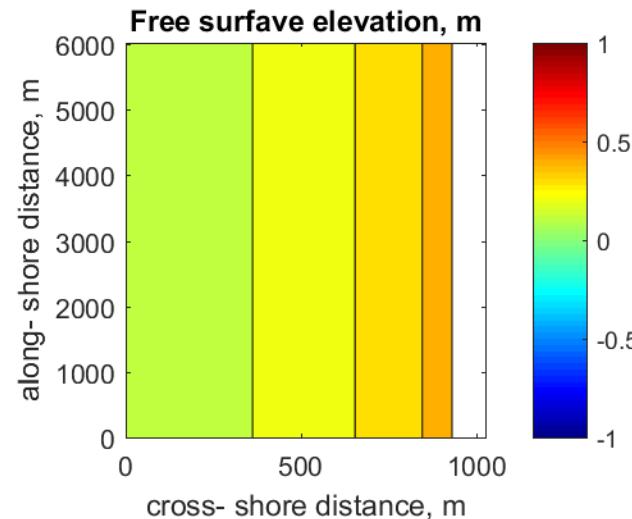
Hout(idACen) == T	! AC	3D wave action
Hout(idACcx) == T	! Cx	2D Group velocity in xi dimension
Hout(idACcy) == T	! Cy	2D Group velocity in etai dimension
Hout(idACct) == T	! Ct	2D Group velocity in the directional dimension
Hout(idACtp) == T	! Tp	2D Group peak period



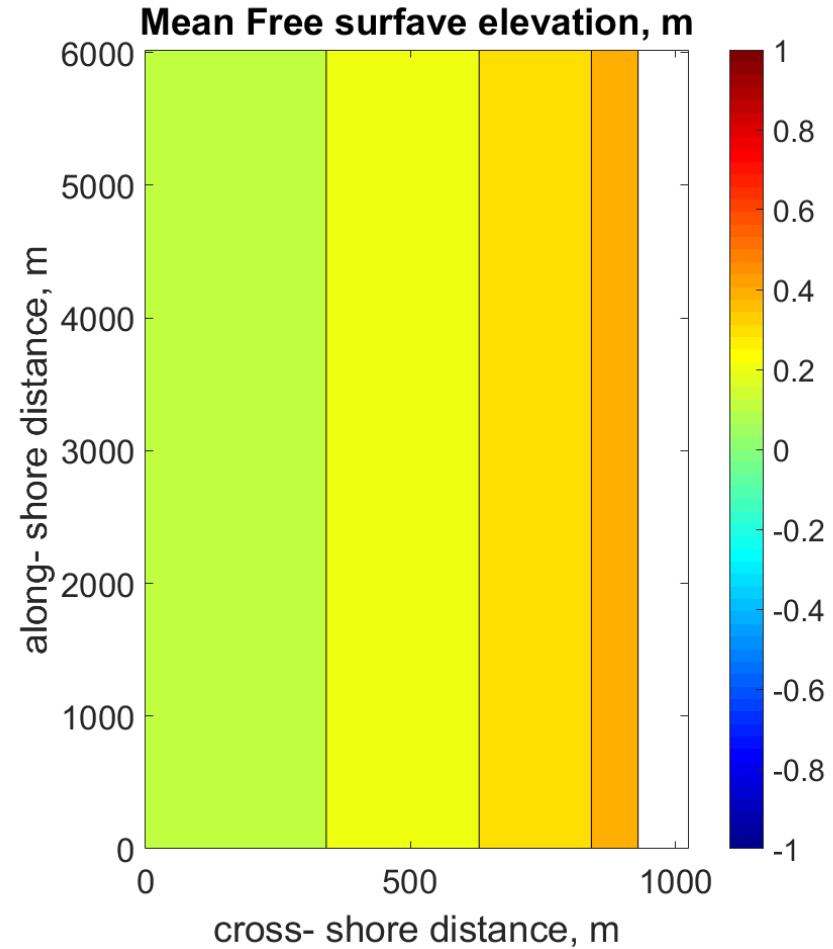
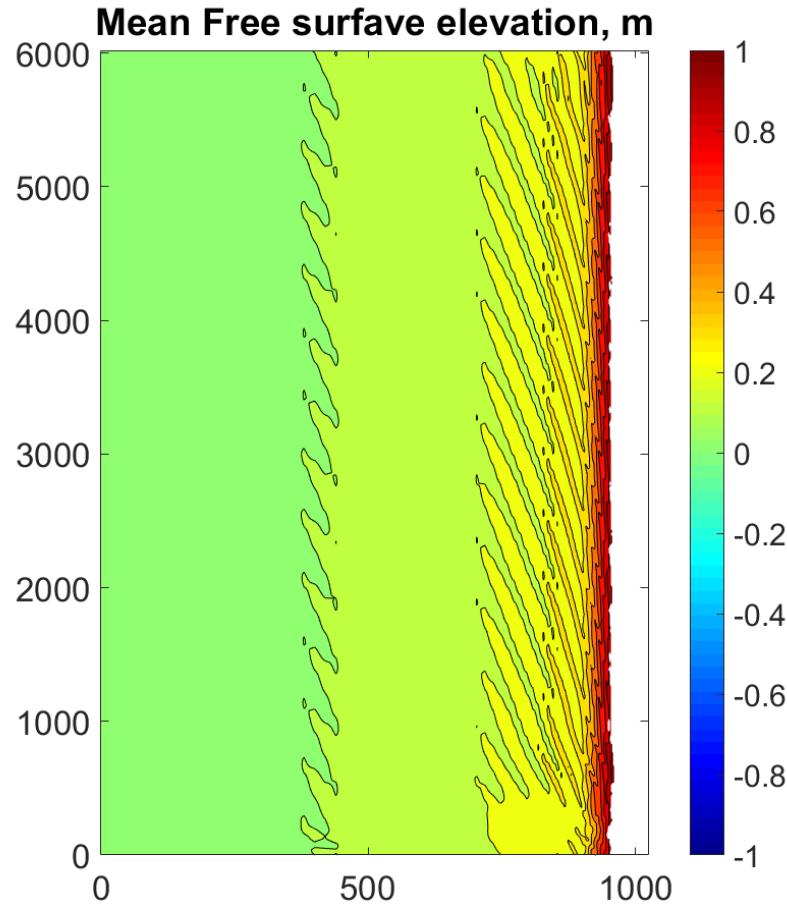
$\beta=1.18$

Steep-slope regime: breakpoint generation dominance

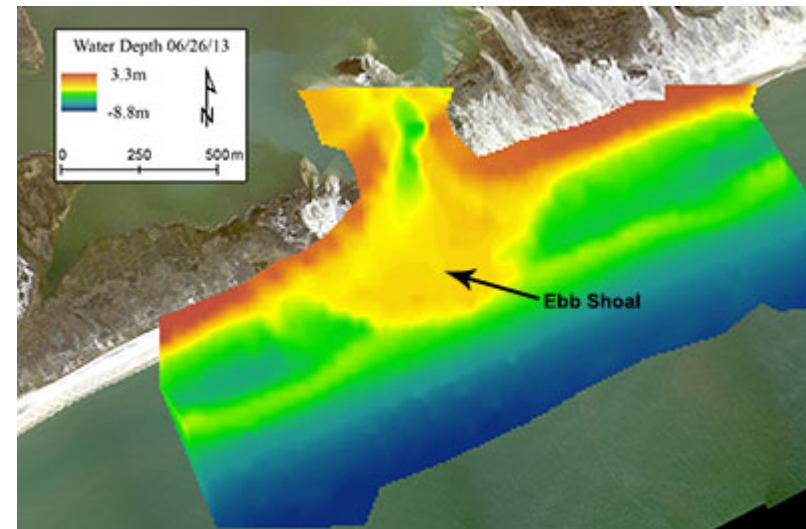
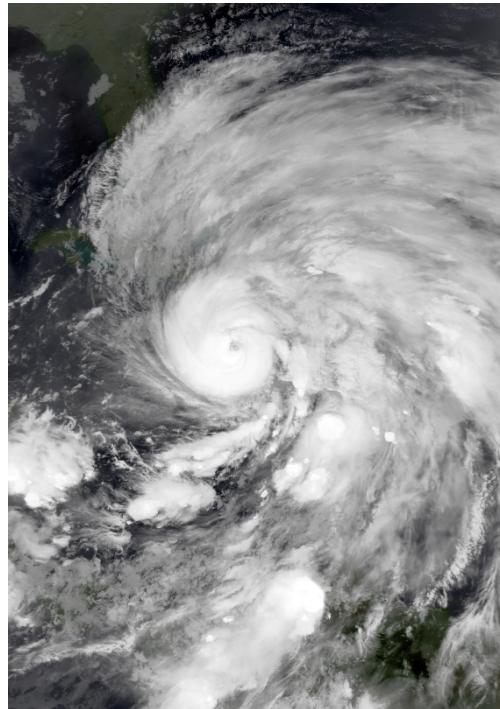
What do we get for the equivalent wave field but without wave-groups?



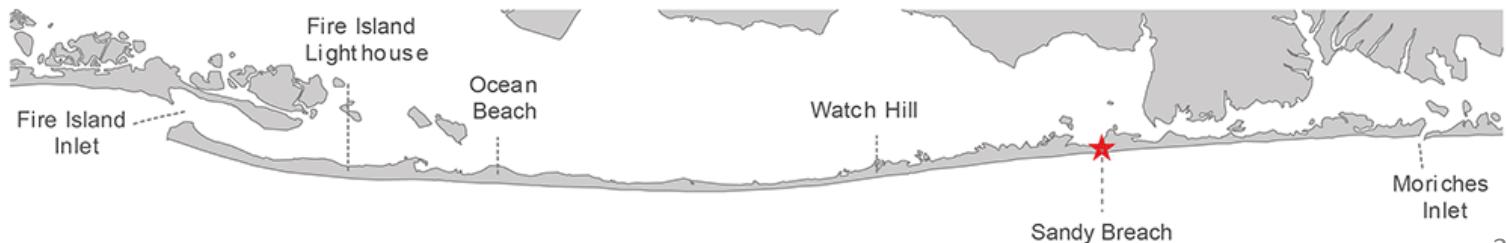
With wave-groups



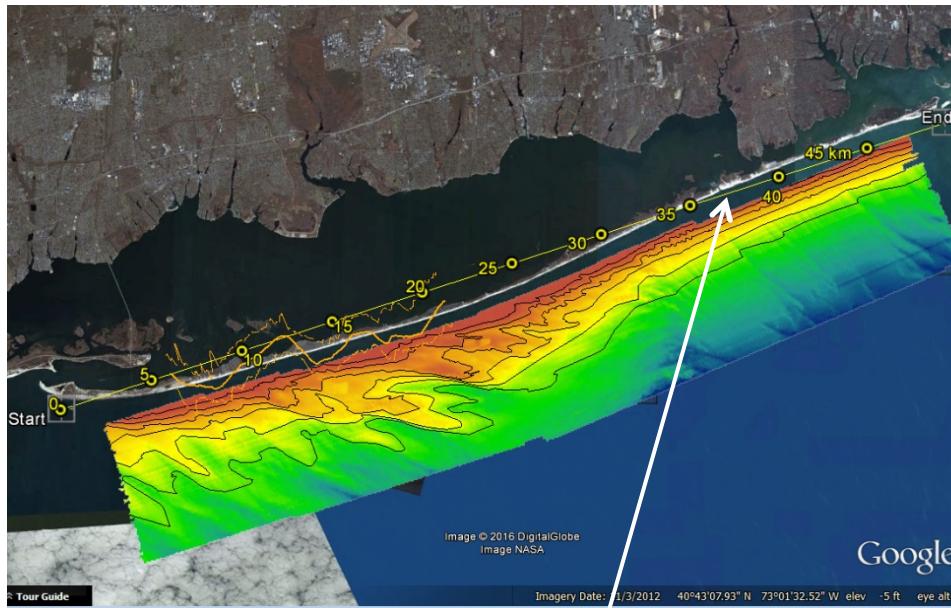
3D CASE REAL APPLICATION: HURRICANE SANDY (2012)



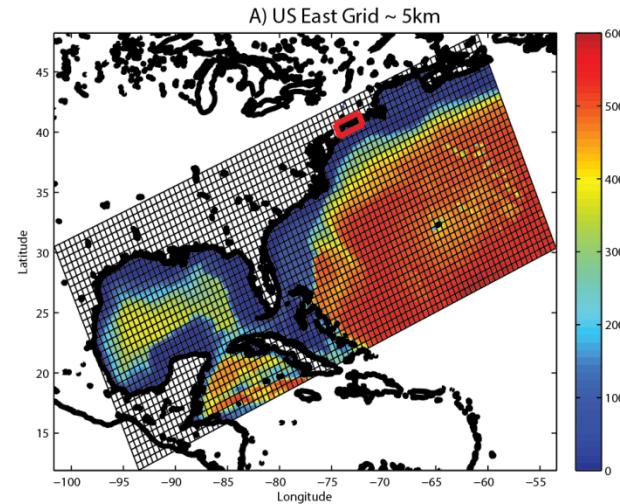
<http://storms.ngs.noaa.gov/storms/sandy/>



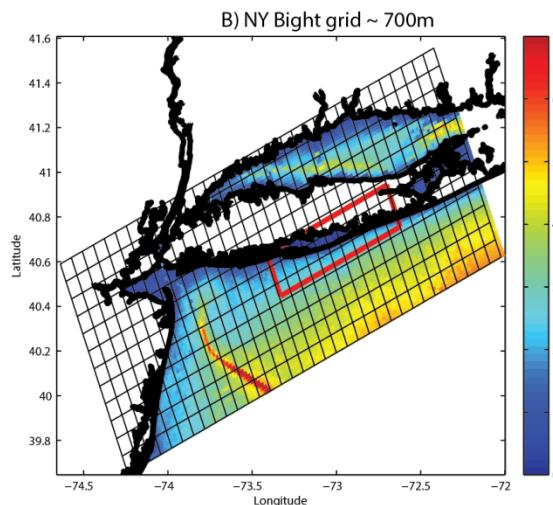
Breach occurred at "Old Inlet" Was open between 1763 and 1827.
Re-opened during H Sandy. Still open today.



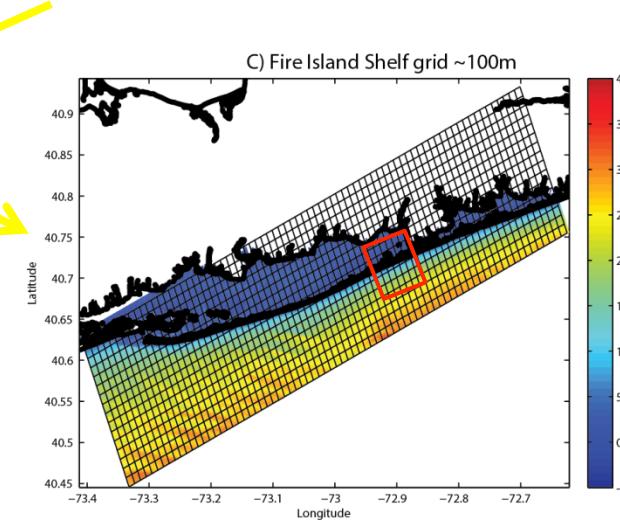
<http://coastal.er.usgs.gov/hurricanes/sandy/photo-comparisons/>



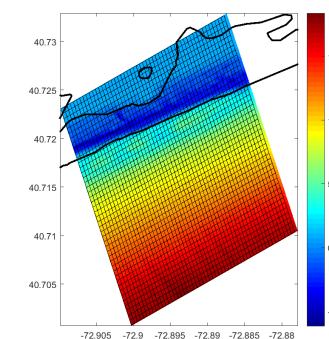
*USEast grid
(5-km res.)*



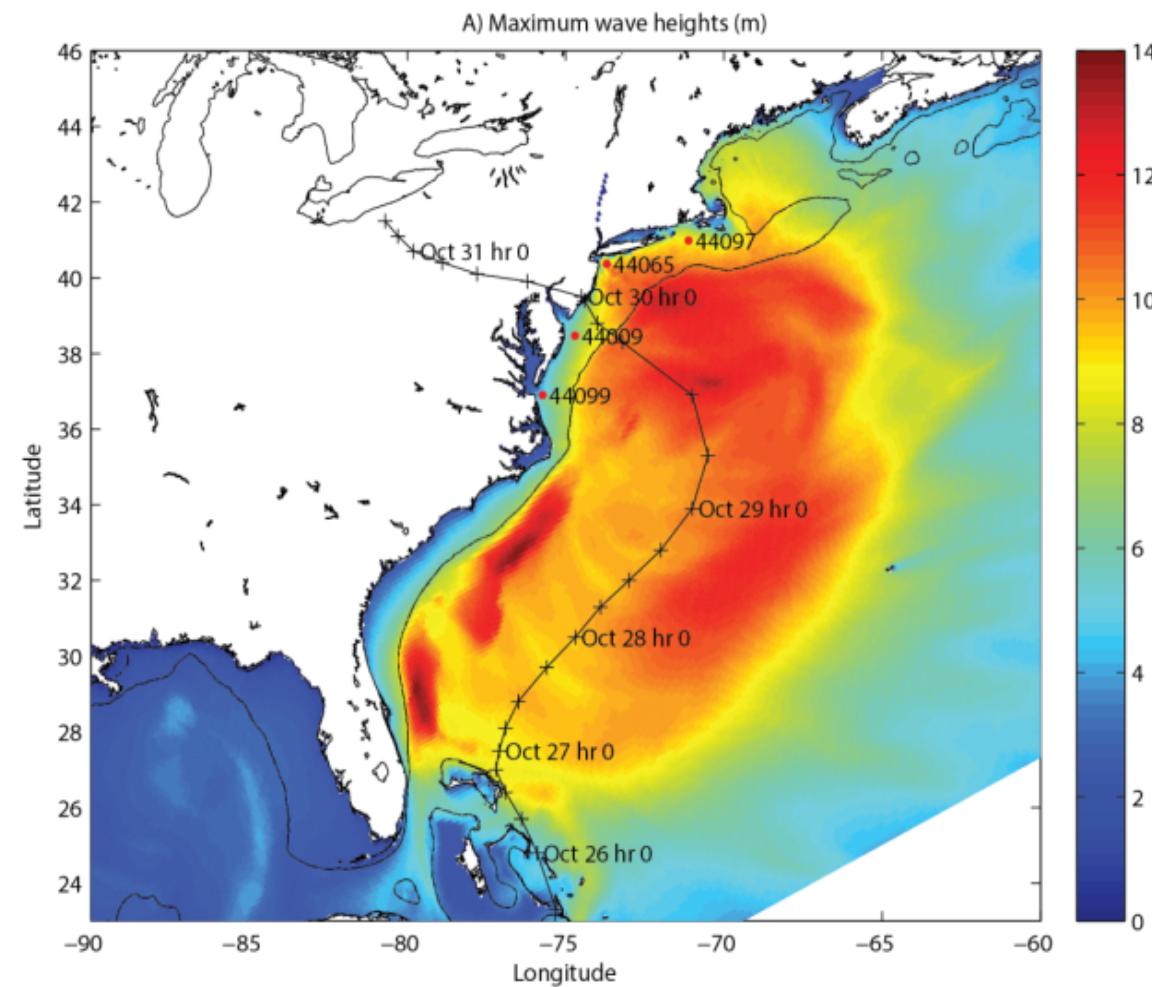
*New York Bright
grid (700-m res.)*

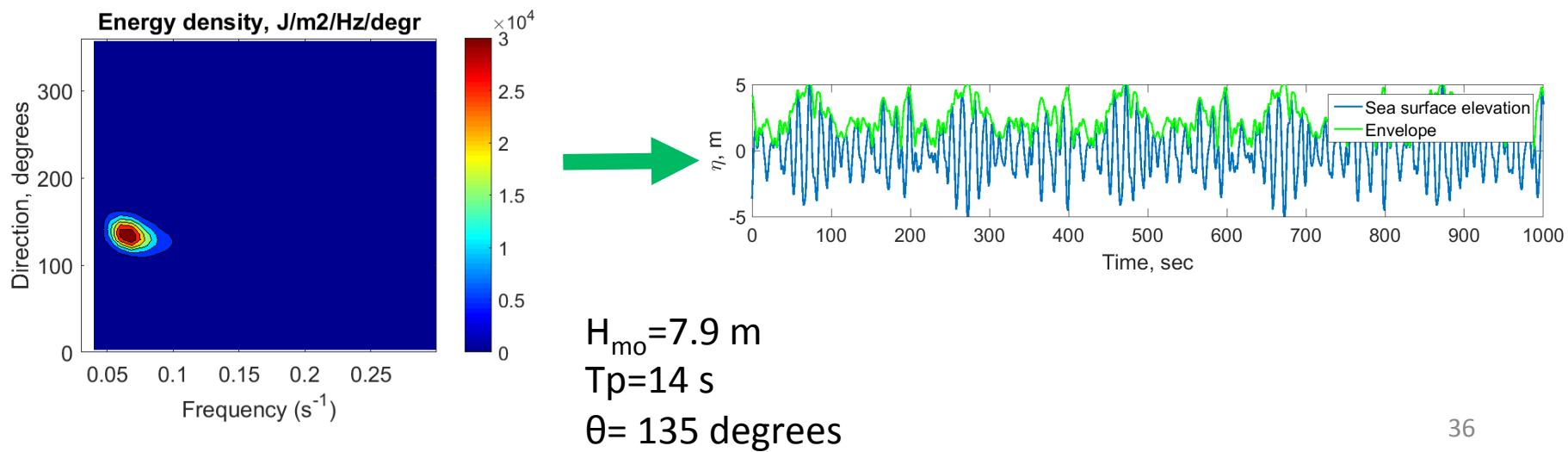
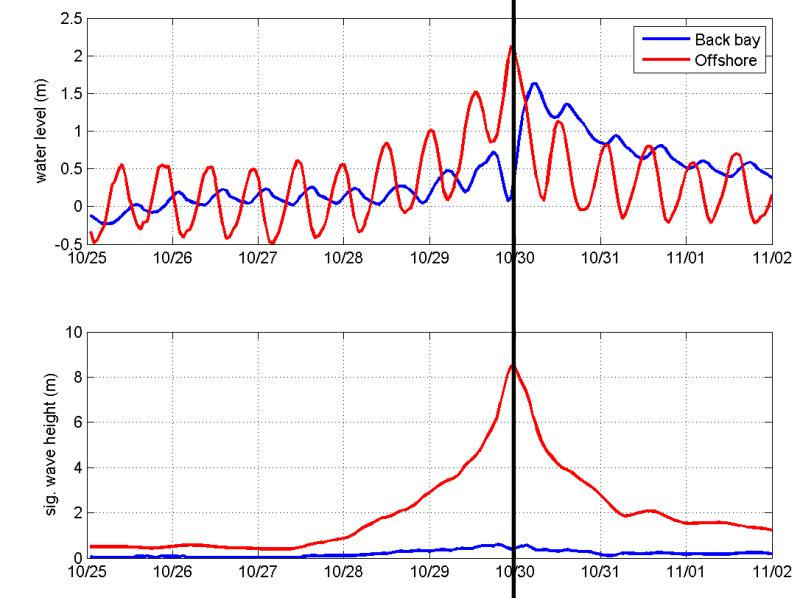
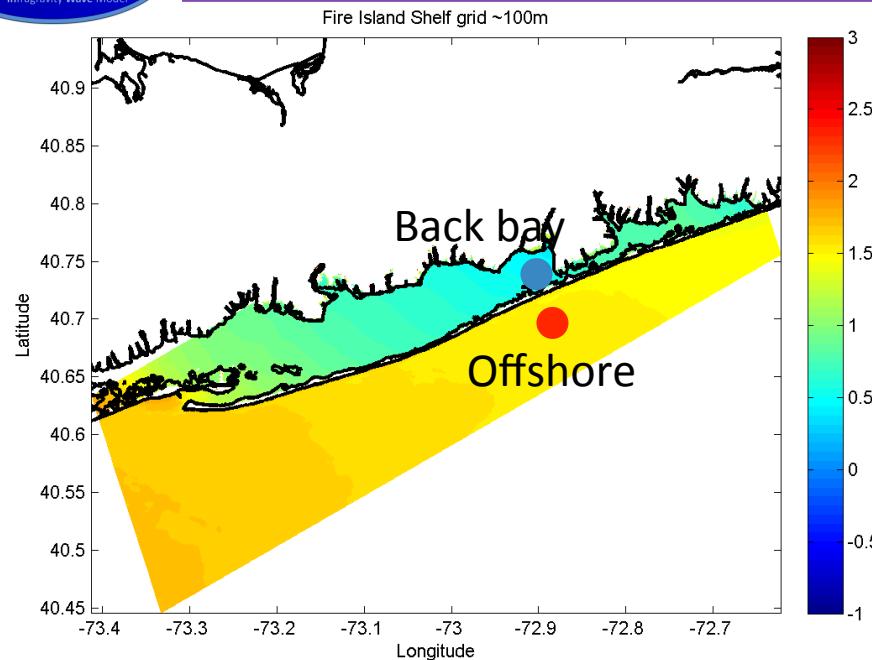


*Shelf grid
(100-m res.)*



*Breach grid
(5-10 m res.)*

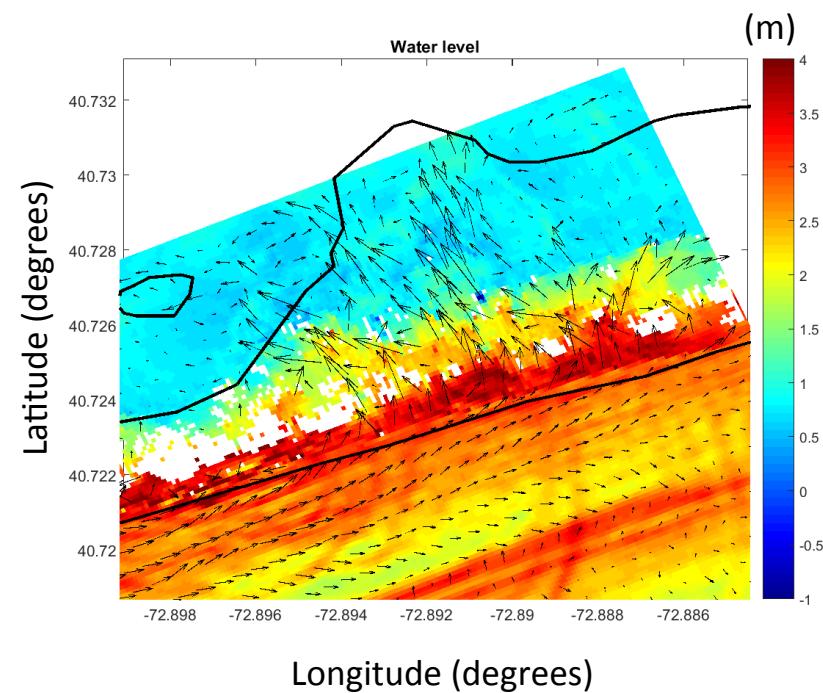
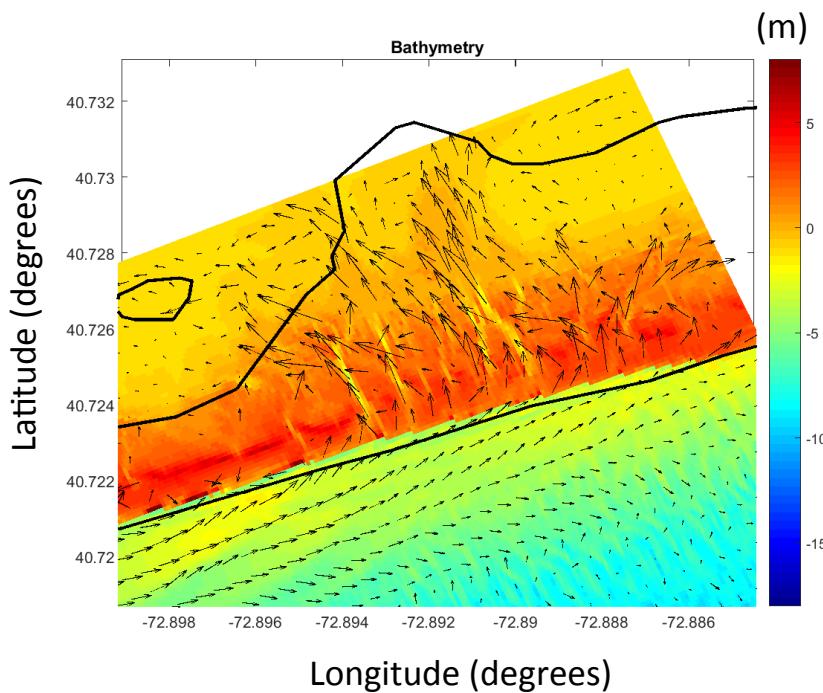
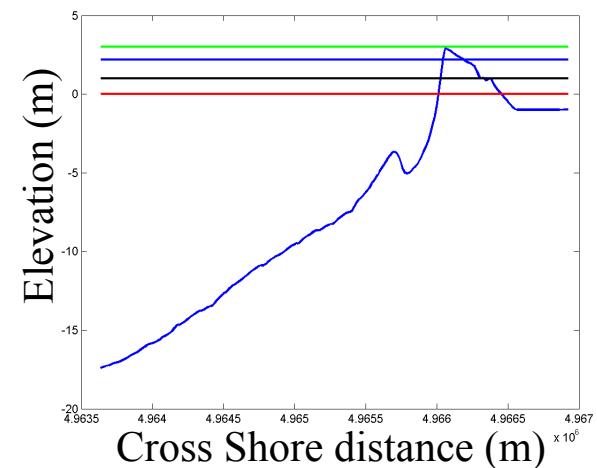






- Infragravity wave (0.8m)
- Surge (1.5m)
- Tide (1.0m)
- MSL (0.0m)

Cross shore profile
near breach location



FUTURE PLANS

- Improve the SWAN-INWAVE interface (still developing and testing it).
- INWAVE is not capable of including wave spectral variations along its boundaries and future efforts will be directed to include these capabilities.
- Validate Inwave with more test cases and field data.
- Include the manual in COAWST_User_Manual.doc