Wave-current Interaction (WEC) in COAWST

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With
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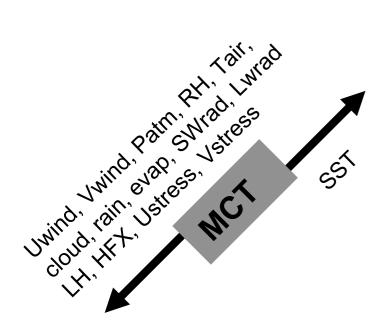
see Kumar et al., 2012:

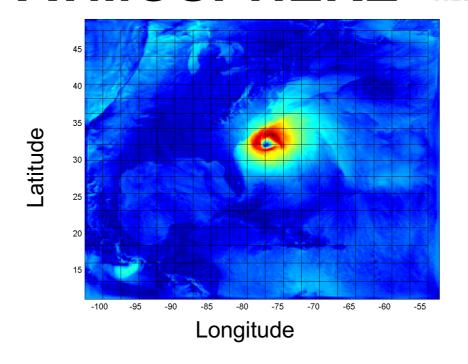
Implementation of the vortex force formalism in the coupled ocean-atmosphere-wave-sediment transport (COAWST) modeling system for inner shelf and surf zone applications, Ocean Modelling, Volume 47, 2012, Pages 65-95, 10.1016/j.ocemod.2012.01.003.

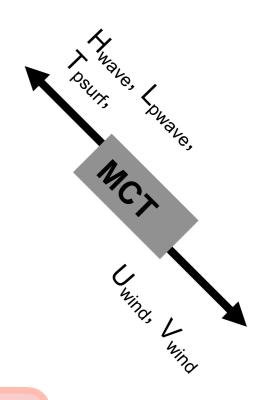


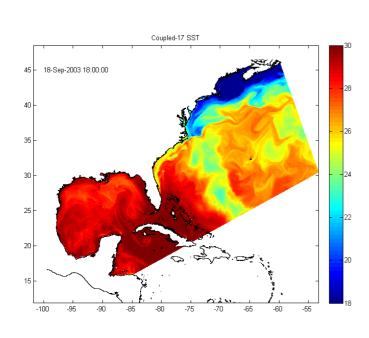
ATMOSPHERE WIRE

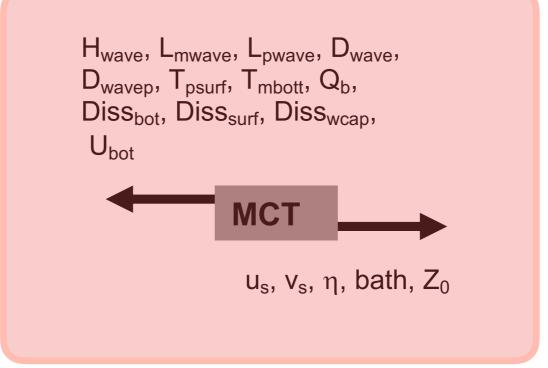


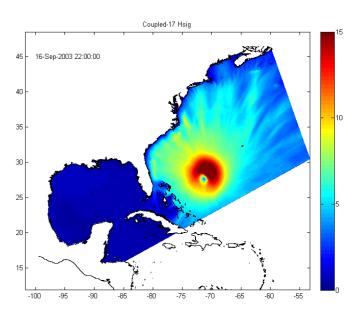
















Wave-Current Interaction Recipes

Mellor Radiation Stress

*see Kumar et al., 2011

Vortex Force Formalism (needs wave dissipation)

*see Kumar et al., 2012

cppdefs.h (COAWST/ROMS/Include)		
WEC_MELLOR	Activates Mellor (2011) method for WEC	
WEC_VF	Activates McWilliams et al. (2004), Uchiyama et al., 2010 for WEC	

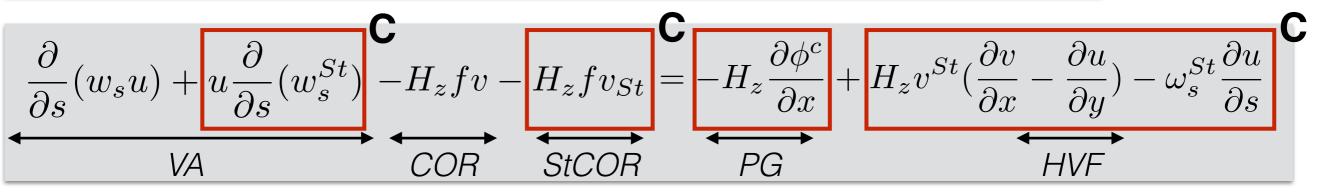
Additional Processes

- Roller Model
- Wave-induced Mixing
- Bottom Streaming
- Surface Streaming

Wave-Averaged Eqs. (WEC_VF, e.g., Eq 11)

$$\frac{\partial}{\partial t}(H_z u) + \frac{\partial}{\partial x}(H_z u \cdot u) + \frac{\partial}{\partial y}(H_z u \cdot v) + u \frac{\partial}{\partial x}(H_z u^{St}) + u \frac{\partial}{\partial y}(H_z v^{St})$$

$$+ ACC \qquad + HA$$



$$+H_zF^x + H_zF^{wx} + H_zD^x - \frac{\partial}{\partial s}(u^{\bar{t}}v' - \frac{\nu}{H_z}\frac{\partial u}{\partial s})$$

$$U^{St} = \text{Stokes drift}$$

$$u = \text{Eulerian mean}$$

Wave-current Interaction Terms

StCOR Stokes-Coriolis Force

PG

Pressure Gradient (includes Bernoulli head, quasi-static pressure etc.)

HVF Horizontal Vortex Force

BA, RA Breaking and Roller Accelerations

Str Bottom and Surface Streaming

Breaking Acceleration F_{wx} Depth-limited Wave-Dissipation Options

 WEC_VF option requires depth-limited dissipation to estimate breaking acceleration (similar to radiation stress gradients).

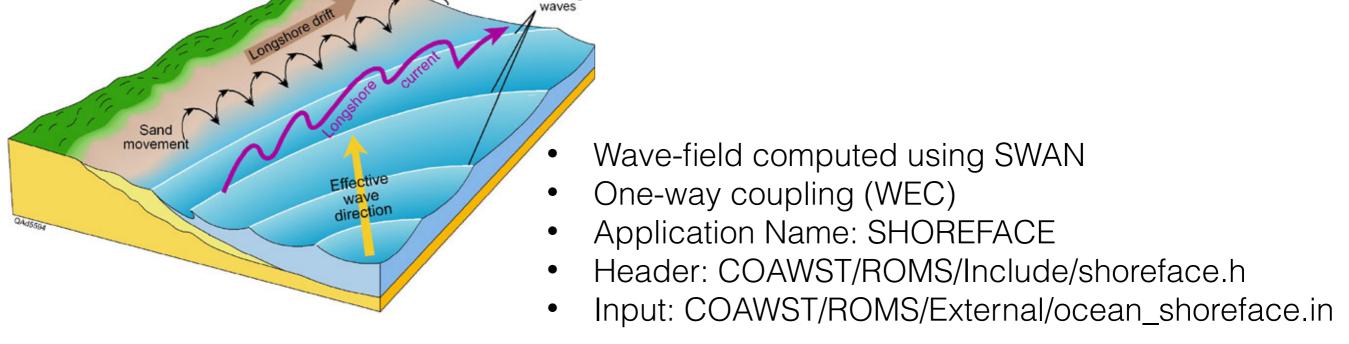
Dissipation Options		
WDISS_THORGUZA	Depth-limited wave dissipation from Thornton & Guza (1983), see Eq. 31.	
WDISS_CHURTHOR	Depth-limited wave dissipation from Church & Thornton (1993), see Eq. 32	
WDISS_WAVEMOD	Depth-limited wave dissipation from SWAN. Use INRHOG=1	

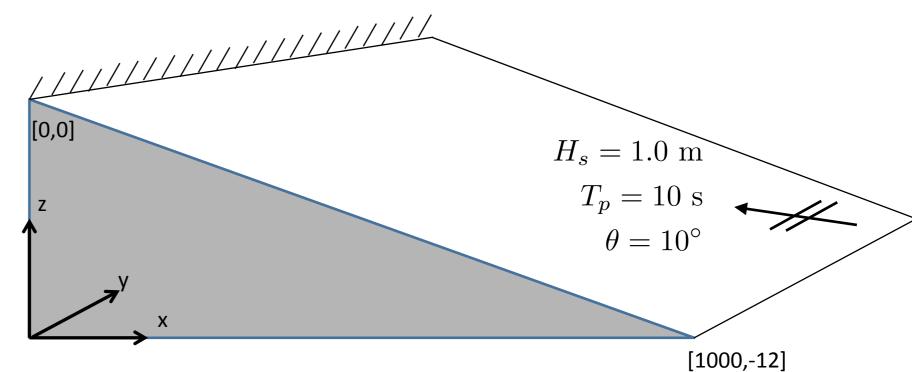
Notes:

- If no wave-dissipation information available use WDISS_THORGUZA/ CHURTHOR
- If no wave-dissipation module is defined and WEC_VF is still activated, the model expects a forcing file with relevant wave quantities. Codes available for this in /COAWST/Tools/mfiles/

Shoreface Test Case (Obliquely Incident Waves on a Planar Beach)

Crests of





Header File (COAWST/ROMS/Include/shoreface.h)

```
svn $Id: shoreface.h 429 2009-12-20 17:30:26Z arango $
   Copyright (c) 2002-2014 The ROMS/TOMS Group
     Licensed under a MIT/X style license
     See License_ROMS.txt
   Options for Shore Face Planar Beach Test Case.
**
  Application flag:
                      SHOREFACE
   Input scripts: ocean_shoreface.h
                       sediment_shoreface.h
*/
#define ROMS_MODEL
#undef WEC_MELLOR
#define WEC_VF
#define WDISS_CHURTHOR
#define BOTTOM_STREAMING
                               → Do not use if not really studying streaming processes
#define SURFACE_STREAMING
```

Input File & Breaking Acceleration (COAWST/ROMS/External/ocean_shoreface.in)

```
! Wec boundary conditions
```

```
LBC(isU2Sd) ==
                                                      ! 2D U-stokes
                         Clo
                                 Gra
                                         Gra
                 Gra
LBC(isV2Sd) ==
                 Gra
                         Clo
                                 Gra
                                         Gra
                                                      ! 2D V-stokes
LBC(isU3Sd) ==
                 Gra
                         Clo
                                         Gra
                                                      ! 3D U-stokes
                                 Gra
LBC(isV3Sd) ==
                                                      ! 3D V-stokes
                         Clo
                 Gra
                                 Gra
                                         Gra
```

! Constants used in surface turbulent kinetic energy flux computation.

```
CHARNOK_ALPHA == 1400.0d0 ! Charnok surface roughness

ZOS_HSIG_ALPHA == 0.5d0 ! roughness from wave amplitude

SZ_ALPHA == 0.25d0 ! roughness from wave dissipation

CRGBAN_CW == 100.0d0 ! Craig and Banner wave breaking

WEC_ALPHA == 0.0d0 ! 0: all wave dissip goes to break and none to roller.

! 1: all wave dissip goes to roller and none to breaking.
```

Breaking Acceleration Term (part of F_{wx})

$$B^b = \frac{(1 - \alpha^r)\epsilon^b}{\rho_0 \sigma} \mathbf{k} \cdot f^b(z)$$

 $\epsilon_b = \text{Depth-limited dissipation}$

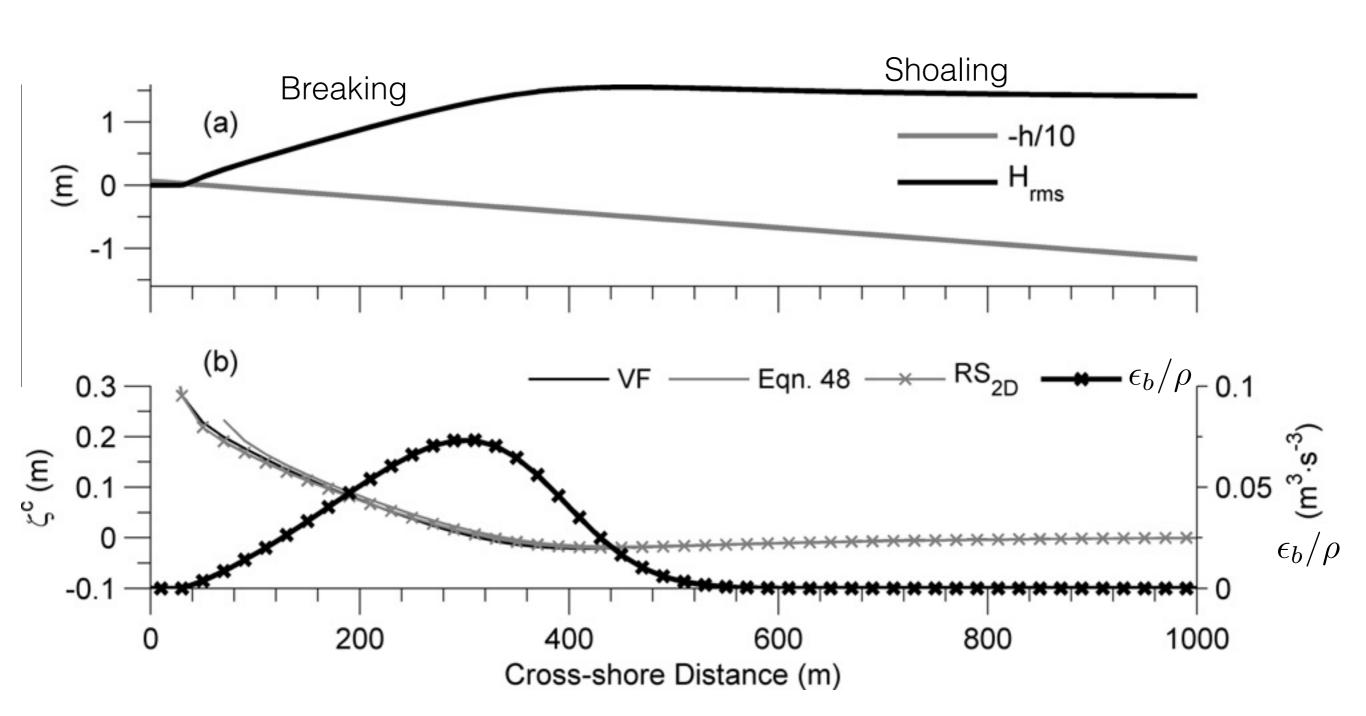
WEC Related OUTPUT

(COAWST/ROMS/External/ocean_shoreface.h)

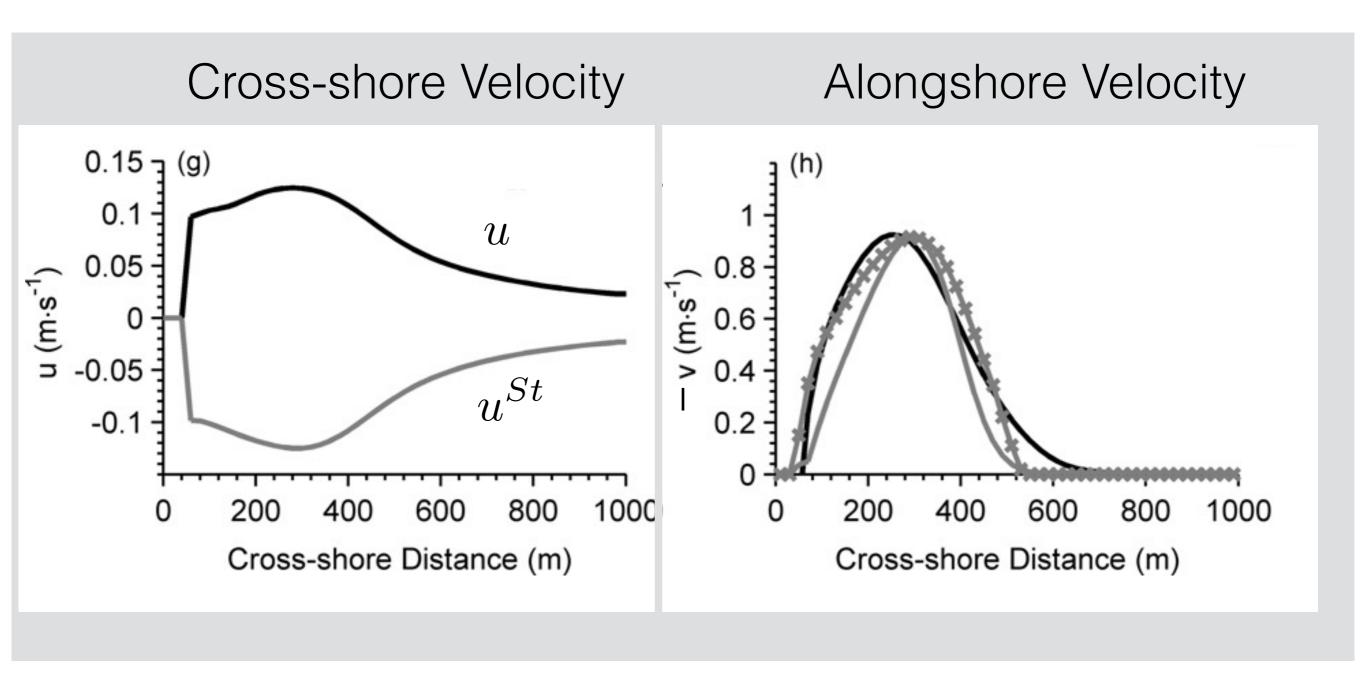
```
Hout(idU2Sd) == T
                        ! ubar_stokes
                                              2D U-Stokes velocity
Hout(idV2Sd) == T
                                              2D V-Stokes velocity
                        ! vbar_stokes
Hout(idU3Sd) == T
                                              3D U-Stokes velocity
                        ! u_stokes
Hout(idV3Sd) == T
                                              3D V-Stokes velocity
                        ! v stokes
Hout(idW3Sd) == T
                                              3D Omega-Stokes velocity
                        ! omega_stokes
Hout(idW3St) == T
                        ! w_stokes
                                              3D W-Stokes velocity
Hout(idWamp) == T
                                             wave height
                        ! Hwave
Hout(idWlen) == T
                                             wave length-mean
                        ! Lwave
Hout(idWlep) == T
                                             wave length-peak
                        ! Lwavep
Hout(idWdir) == T
                        ! Dwave
                                             wave direction
Hout(idWptp) == T
                                             wave surface period
                        ! Pwave_top
                                             wave bottom period
Hout(idWpbt) == T
                        ! Pwave_bot
Hout(idWorb) == T
                                              wave bottom orbital velocity
                        ! Uwave_rms
Hout(idWbrk) == T
                                              wave breaking (percent)
                        ! Wave_break
Hout(idUwav) == T
                                              wave-depth avgeraged U-velocity
                        ! uWave
Hout(idVwav) == T
                                              wave-depth avgeraged V-velocity
                        ! vWave
                                              wave dissipation due to bottom friction
Hout(idWdif) == T
                        ! Dissip_fric
Hout(idWdib) == T
                        ! Dissip_break
                                              wave dissipation due to breaking
Hout(idWdiw) == T
                        ! Dissip_wcap
                                              wave dissipation due to white capping
                        ! Dissip_roller
Hout(idWdis) == T
                                              wave roller dissipation
Hout(idWrol) == T
                                              wave roller action density
                        ! rollA
```

Shoreface Test Results

← Wave propagation direction

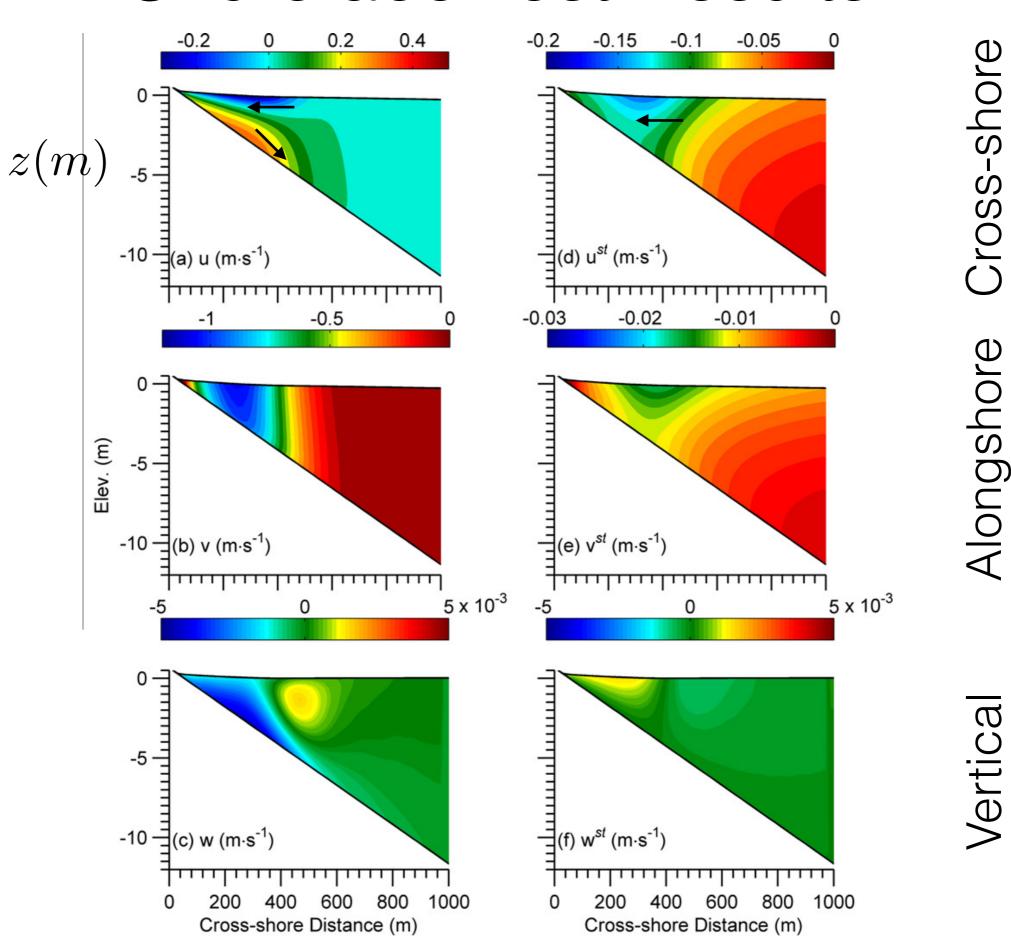


Shoreface Test Results (Depth-averaged)



$$u^{St}$$
 = Stokes drift
 u = Eulerian mean

Shoreface Test Results



Roller Model Options

Roller Options		
ROLLER_SVENDSEN	Activates wave rollers based on Svendsen, 1984. See Warner et al. (2008), Eqns. 7 and 10.	
ROLLER_MONO	Activates wave roller for monochromatic waves from REF/DIF. See Haas and Warner, 2009.	
ROLLER_RENIERS	Activates wave rollers following Reniers et al. (2004). See equations 34-39.	

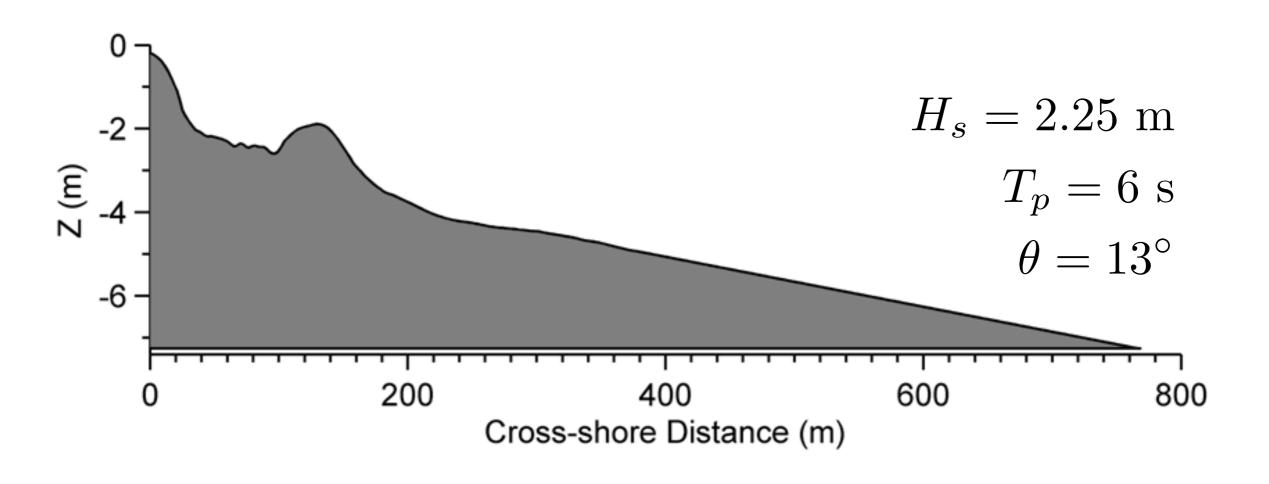
Notes:

 If ROLLER_RENIERS is activated then the parameter wec_alpha in the INPUT file must be changed. For wec_alpha=0 no wave-dissipation goes into creating rollers, while for wec_alpha=1 all wave dissipation creates rollers

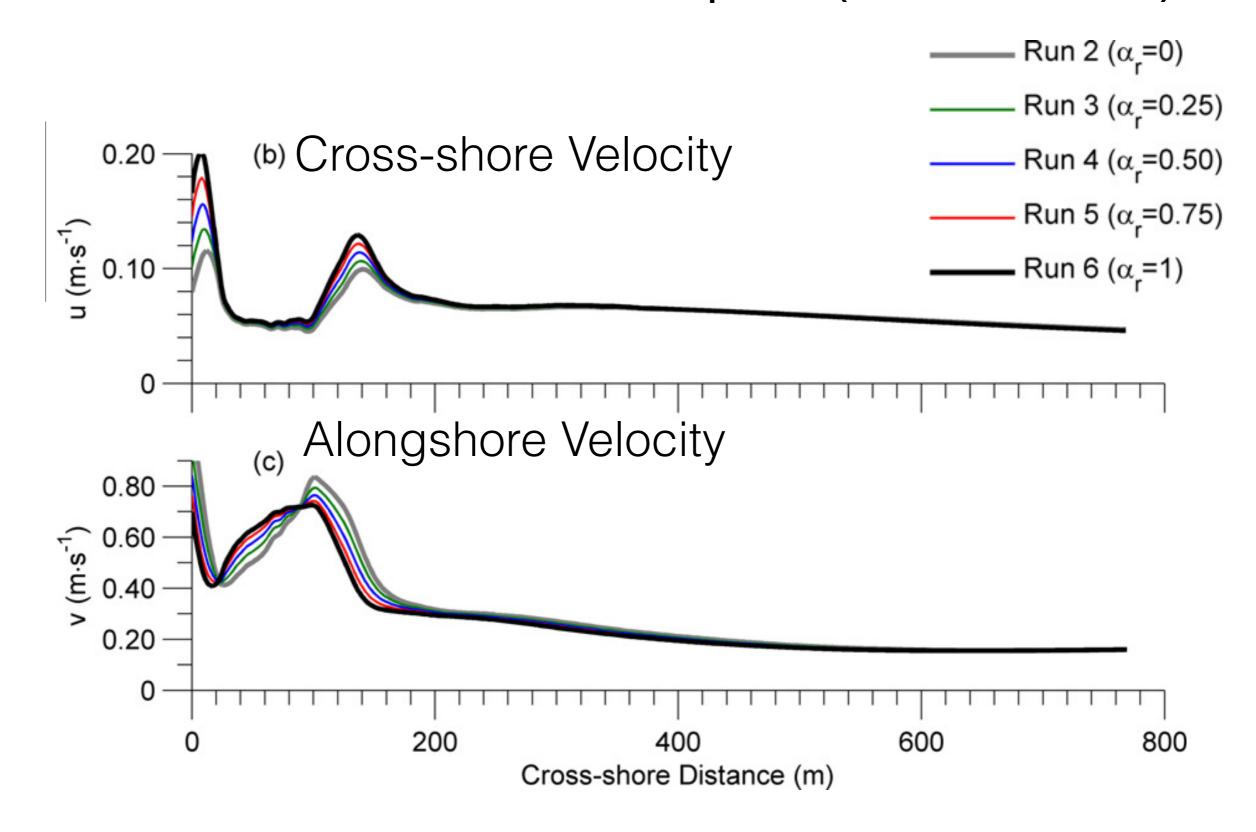
```
WEC_ALPHA == 0.0d0 ! 0: all wave dissip goes to break and none to roller.
! 1: all wave dissip goes to roller and none to breaking.
```

DUCK'94 Test Case

(Obliquely Incident Waves on a Barred Beach)



Roller Reniers Example (DUCK'94)



Wave-induced Mixing (within GLS)

Mixing Options

TKE_WAVEDISS ZOS_HSIG

Inputs part of wave-energy dissipation as near surface TKE. See equations 44-47.

The option ZOS_HSIG indicates that (a) the surface roughness or mixing length is provided as percent of wave height (see equation 46); (b) the amount of energy as TKE is provided as percent of wave dissipation (see equation 47).

$$K_v \frac{\partial k}{\partial z}|_{z=\zeta} = c_{\epsilon w} \epsilon_w$$

$$ZOS_HSIG_ALPHA == 0.5d0$$

 $SZ_ALPHA == 0.25d0$

! roughness from wave amplitude ! roughness from wave dissipation

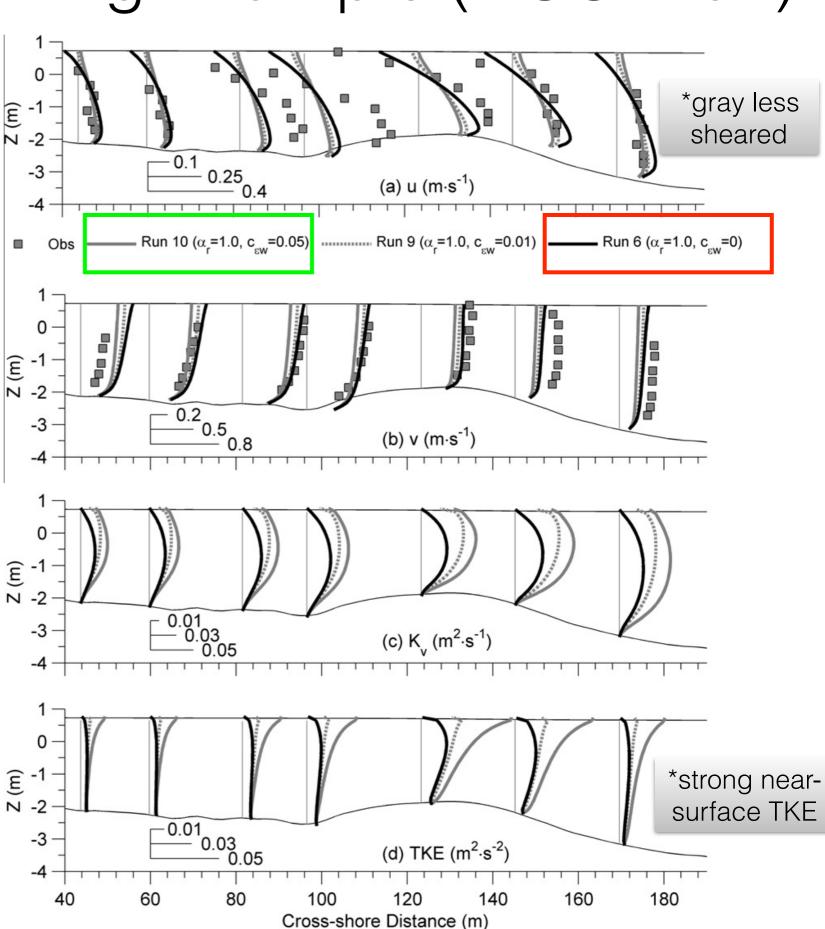
Wave-induced Mixing Example (DUCK' 94)

Cross-shore Velocity

Alongshore Velocity

Vertical eddy viscosity

Turbulent Kinetic Energy



Bottom and Surface Streaming

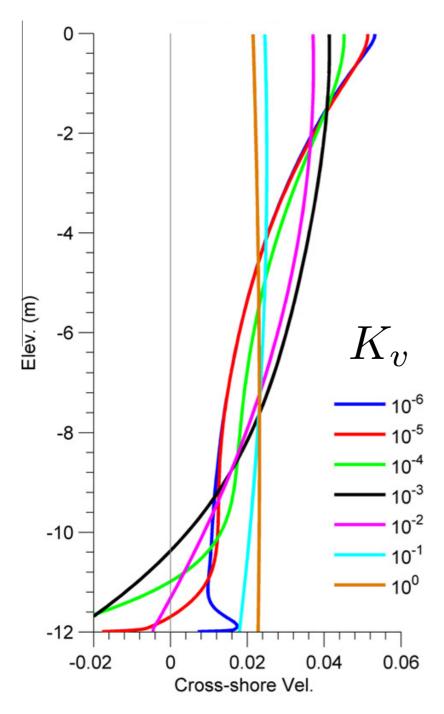
Streaming Options		
BOTTOM_STREAMING	Wave-induced bottom streaming based on Reniers et al. (2004). Requires bottom friction induced wave-dissipation	
BOTTOM_STREAMING_ XU_BOWEN	Estimates bottom streaming based on Xu & Bowen (1994)	
SURFACE_STREAMING	Estimates surface streaming based on Xu & Bowen (1994)	

Notes:

• If BOTTOM_STREAMING_XU_BOWEN is activated, the wave-bottom boundary layer needs to be resolved, which requires very high near-bottom resolution. Suggested **VTRANSFORM=2** and **VSTRETCHING=3**

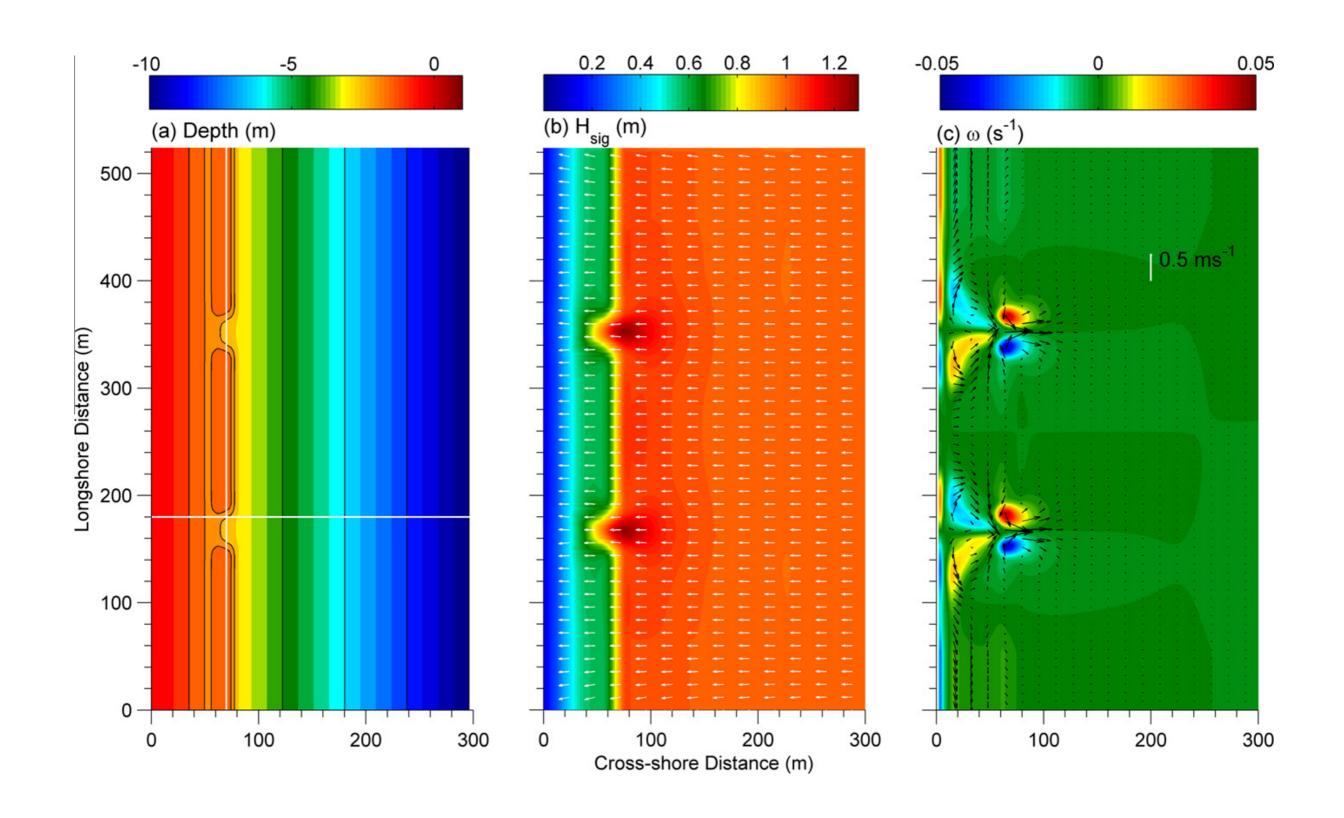
Bottom Streaming (Inner-shelf Undertow)

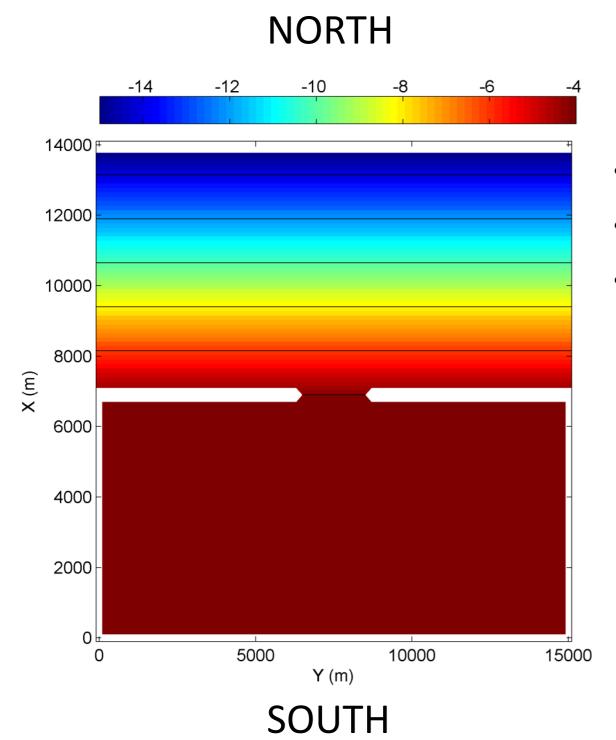
Offshore-Directed Undertow



^{*}for small Kv, cross-shore velocity u is sheared and similar to Stokes-drift $u^{\rm St}$ indicating balance between Coriolis and Stokes-Coriolis forces $f_{\rm cor}u=f_{\rm cor}u^{\rm St}$

Rip-Current Dynamics





Inlet Test Case

- Wave field computed using SWAN
- Two way coupling (WEC and CEW)
- Application Name: INLET_TEST

Header file: COAWST/Projects/Inlet_test/Coupled/inlet_test.h

Input file: COAWST/Projects/Inlet_test/Coupled/ocean_inlet_test.in

COAWST/Projects/Inlet_test/Coupled/swan_inlet_test.in

COAWST/Projects/Inlet_test/Coupled/coupling_inlet_test.h

Inlet Test Case- Header File

```
#define ROMS MODEL
#define SWAN MODEL
#define MCT LIB
#define UV_VIS2
#define MIX_S_UV
#define MASKING
#define UV_ADV
#undef UV_COR
#define TS_MPDATA
#define DJ_GRADPS
#define SPLINES_VDIFF
#define SPLINES_VVISC
#define SOLVE3D
#undef WEC_MELLOR
#define WEC VF
#define WDISS_WAVEMOD
#define UV_KIRBY
#define ANA_INITIAL
#define ANA SMFLUX
#define ANA_FSOBC
#define ANA_M20BC
```

Inlet Test Case- SWAN Input File

```
PROJECT 'Inlet Test' ' '
 'INLET test'
 'Bathymetry: flat bottom'
 'COMMENTS'
MODE NONSTATIONARY TWODIMENSIONAL
SET DEPMIN 0.10 INRHOG 1 NAUTICAL
COORDINATES CARTESIAN
&& KEYWORD for number of nested SWAN grids.
NSGRIDS 1
&& KEYWORDS TO CREATE AND READ COMPUTATIONAL GRID &&
CGRID CURVILINEAR 76 71 EXC 9.999000e+003 &
        CIRCLE 36 0.04 1.0 20
READGRID COORDINATES 1 'Projects/Inlet_test/Coupled/inlet_test_grid_coord.grd' 4 0 0 FREE
&& KEYWORDS TO CREATE AND READ BATHYMETRY GRID &&
INPGRID BOTTOM CURVILINEAR 0 0 76 71 EXC 9.999000e+003
READINP BOTTOM 1 'Projects/Inlet_test/Coupled/inlet_test_bathy.bot' 4 0 FREE
&& KEYWORD TO CREATE CURRENT GRID &&
                                                                     &
INPGRID CURRENT CURVILINEAR 0 0 76 71 EXC 9.999000e+003
       NONSTAT 20000101.000000 25 DAY 20000126.000000
&& KEYWORD TO CREATE WATER LEVEL GRID &&
INPGRID WLEV CURVILINEAR 0 0 76 71 EXC 9.999000e+003
                                                                     &
       NONSTAT 20000101.000000 25 DAY 20000126.000000
&& KEYWORD TO CREATE BOTTOM FRICTION GRID &&
                                                                     &
INPGRID FRIC CURVILINEAR 0 0 76 71 EXC 9.999000e+003
       NONSTAT 20000101.000000 25 DAY 20000126.000000
&& BOUNDARY FORCING &&
BOUNDPAR1 SHAPESPEC JONSWAP 3.3 PEAK DSPR DEGREES
BOUNDPAR2 SEGMENT IJ 0 71 76 71 CONSTANT PAR 1.0 10.0 0. 20.
```

Inlet Test Case- Coupling File

```
Number of parallel nodes assigned to each model in the coupled system.
! Their sum must be equal to the total number of processors.
 NnodesATM = 0
                                     ! atmospheric model
 NnodesWAV = 1
                                     ! wave model
 NnodesOCN = 1
                                     ! ocean model
 Time interval (seconds) between exchange of fields between models.
 TI_ATM2WAV =
                                      ! atmosphere to wave coupling interval
                  0.0d0
 TI\_ATM20CN =
                  0.0d0
                                      ! atmosphere to ocean coupling interval
 TI WAV2ATM =
                  0.0d0
                                      ! wave to atmosphere coupling interval
 TI WAV20CN =
                                      ! wave to ocean coupling interval
                600,0d0
                                      ! ocean to wave coupling interval
 TI_OCN2WAV =
                600.0d0
 TI_OCN2ATM =
                                      ! ocean to atmosphere coupling interval
                  0.0d0
! Enter names of Atm, Wav, and Ocn input files.
 The Wav program needs multiple input files, one for each grid.
  ATM_name = namelist.input
                                                                   ! WRF input file
  WAV_name = Projects/Inlet_test/Coupled/swan_inlet_test.in
                                                                   ! wave model
  OCN_name = Projects/Inlet_test/Coupled/ocean_inlet_test.in
                                                                  ! ocean model
! Sparse matrix interpolation weights files. You have 2 options:
! Enter "1" for option 1, or "2" for option 2, and then list the
! weight file(s) for that option.
  SCRIP_WEIGHT_OPTION = 1
 Option 1: IF you set "SCRIP_WEIGHT_OPTION = 1", then enter name
           of the single netcdf file containing all the exchange
           weights. This file is created using the code in
           Lib/SCRIP_COAWST/scrip_coawst[.exe]
  SCRIP_COAWST_NAME = Projects/Inlet_test/Coupled/scrip_weights_inlet_test.nc
```

Running Inlet Test Case

./coawst.bash -j N

```
np = number of processors
coawstM = Executable created after compilation
```

Input file = Projects/Inlet_Test/Coupled/coupling_inlet_test.in

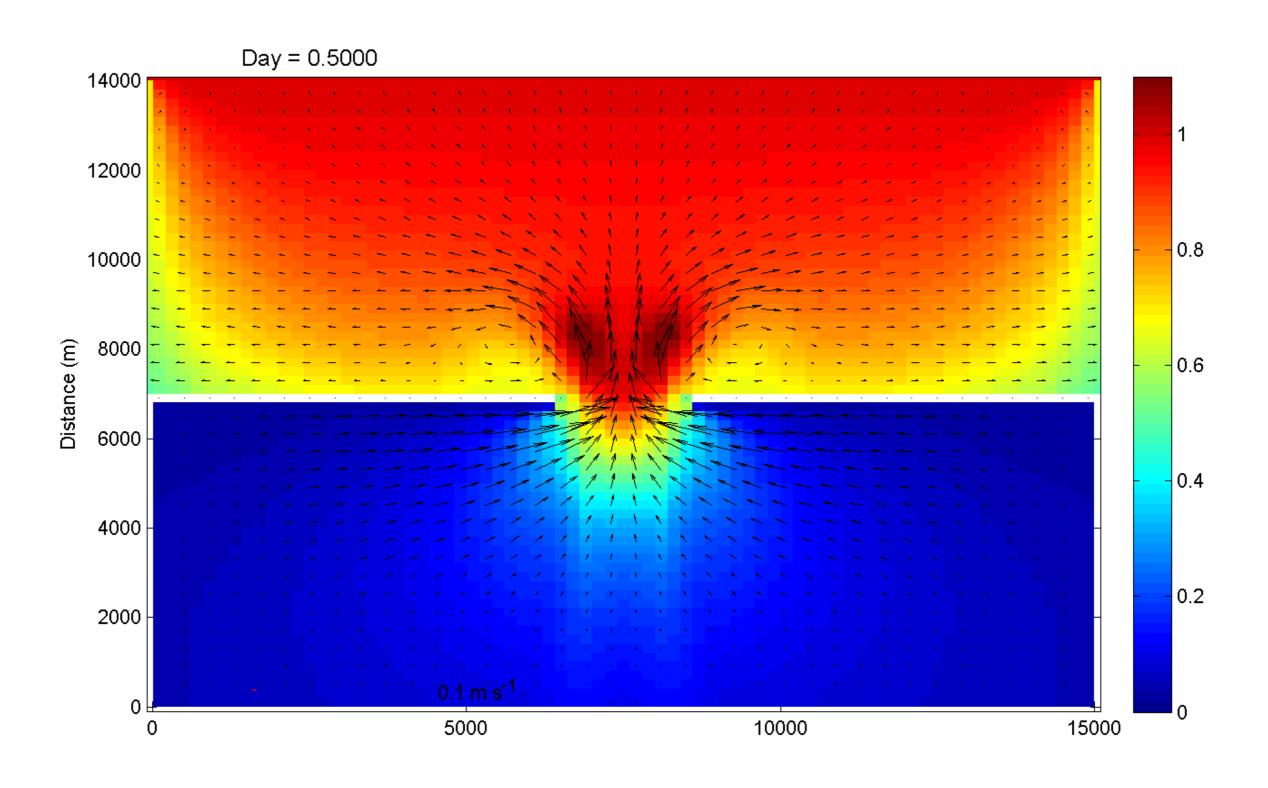
Serial

./coawstS.exe Projects/Inlet_test/Coupled/coupling_inlet_test.in

<u>Parallel</u>

mpiexec/run -np 4 ./coawstM.exe Projects/Inlet_test/Coupled/coupling_inlet_test.in

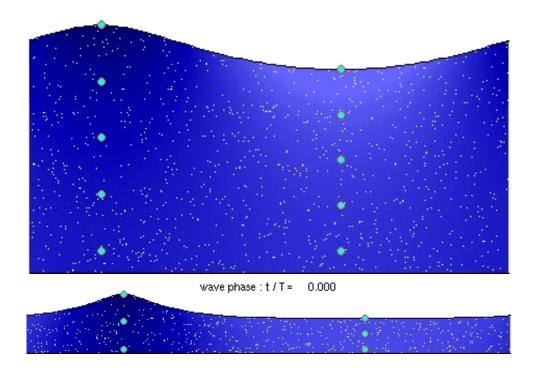
Output Inlet Test Case



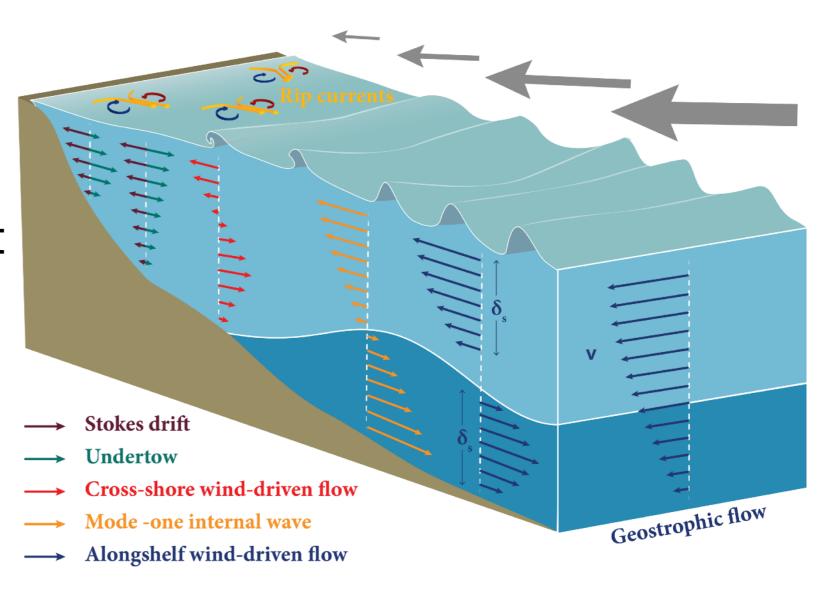
Updated Stokes Drift in COAWST

wave phase : t / T = 0.000

with Guoqiang Liu, Ramsey Harcourt



- Vortex Force
- Langmuir Turbulence
- Cross-shore Transport



Bulk & Spectral Stokes Drift Formulations

$$\mathbf{v}^{\text{St}} = \frac{H_s^2 \omega}{16} \frac{\cosh(2k_{\text{m}}(z+h))}{\sinh^2(k_{\text{m}}h)} \mathbf{k}_{\text{m}}$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

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$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\cosh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\sinh(2k(z+h))}{\sinh^2(kh)} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\sinh(2k(z+h))}{\sinh(2k(z+h))} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\sinh(2k(z+h))}{\sinh(2k(z+h))} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\sinh(2k(z+h))}{\sinh(2k(z+h))} df d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\sinh(2k(z+h))}{\sinh(2k(z+h))} d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\sinh(2k(z+h))}{\sinh(2k(z+h))} d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\sinh(2k(z+h))}{\sinh(2k(z+h))} d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\sinh(2k(z+h))}{\sinh(2k(z+h))} d\theta$$

$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\sinh(2k(z+h))}{\sinh(2k(z+h))} d\theta$$

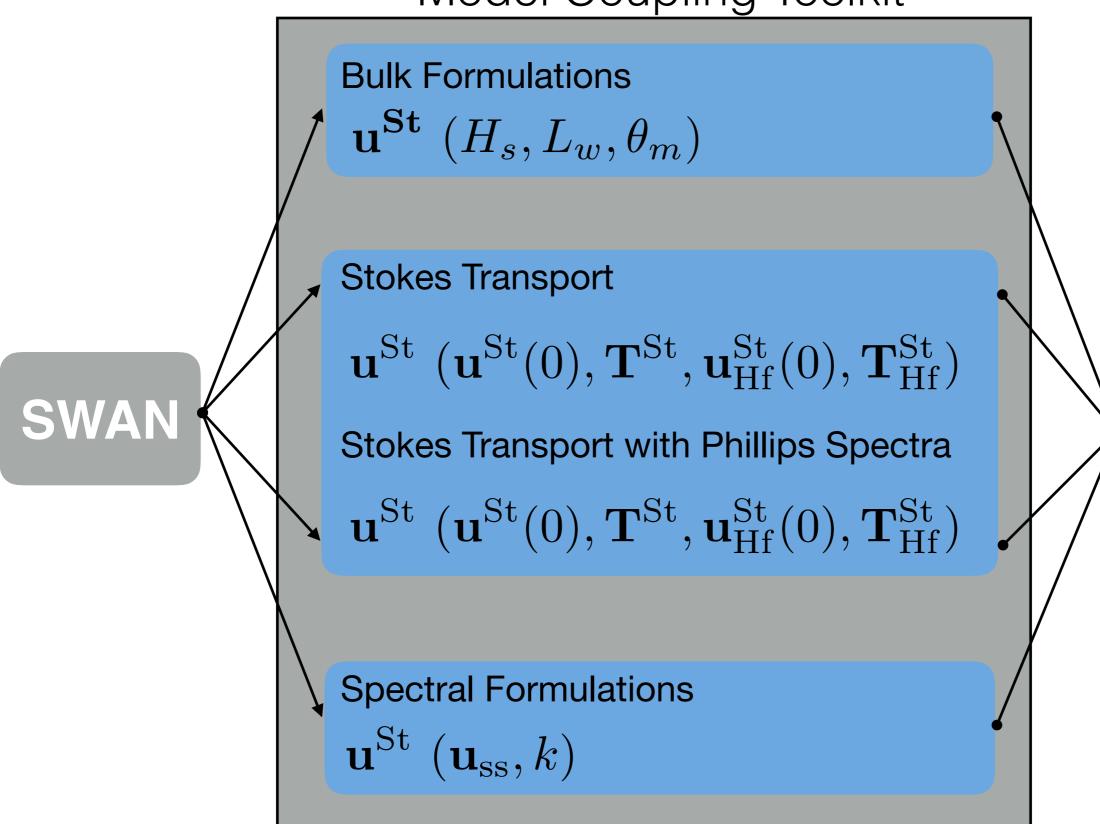
$$\mathbf{v}^{\text{St}} = \int_0^\infty \int_{\theta=0}^{\theta=2\pi} \sigma \mathbf{k} S_{\eta\eta}(f,\theta) \frac{\sinh(2k($$

Dir. $(^{\circ})$

Stokes Vel. (ms^{-1})

Updating Stokes Drift in COAWST



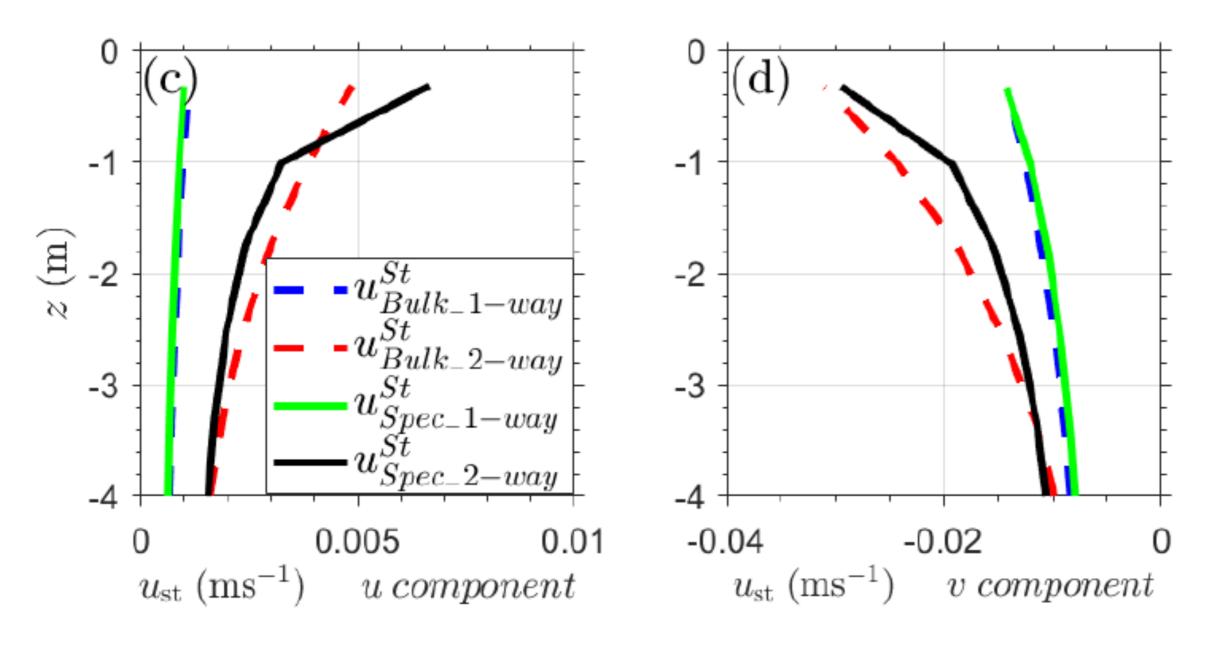


ROMS

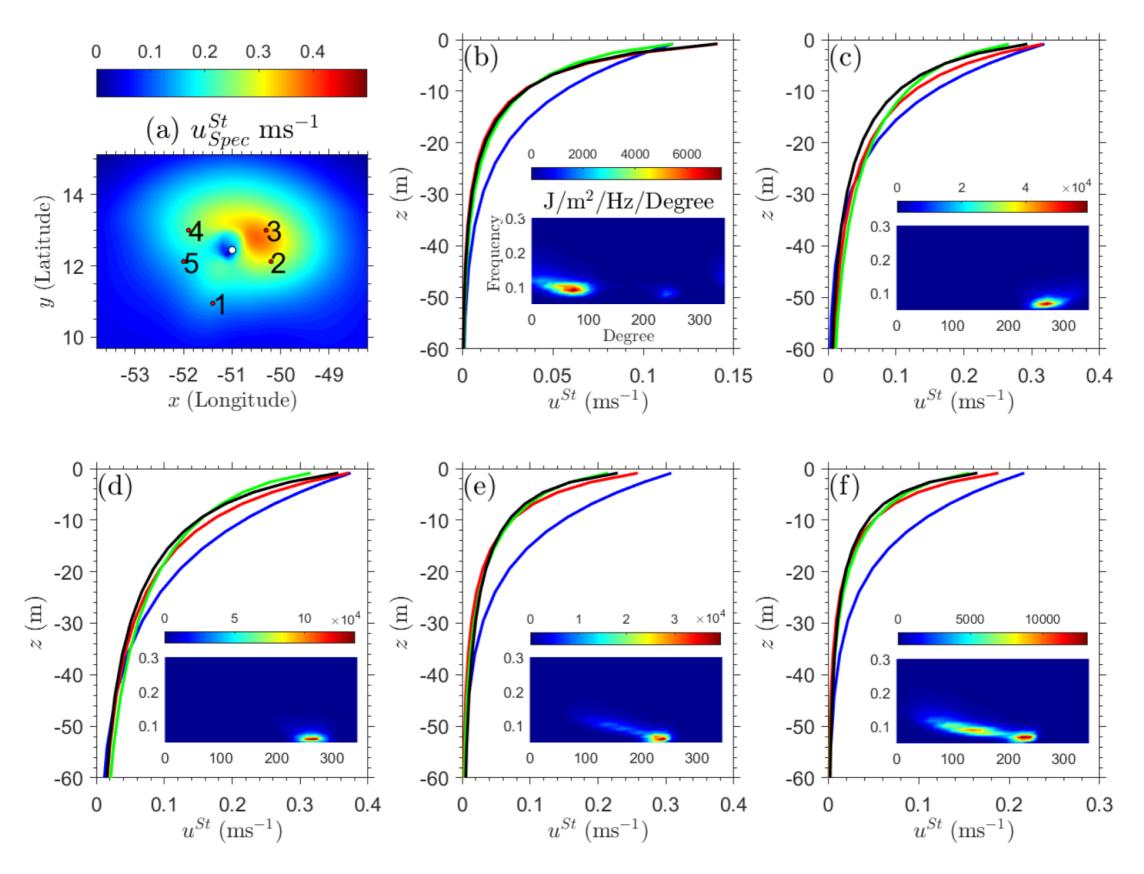
Liu et al., 2019

Inlet Test Case Results

Comparison between Bulk and Spectral Formulations



Idealized Hurricane Test Case



Liu et al., 2019

Second-Moment Closure Modification: Craik-Leibovich Vortex Force

Hydrostatic Primitive Equations

$$\frac{\partial U_i}{\partial t} + U_j \frac{\partial U_i}{\partial x_j} + 2\epsilon_{ijl}\Omega_j U_l = -\frac{1}{\rho_0} \frac{\partial P}{\partial x_i} - g_i \frac{\rho}{\rho_0} - \frac{\partial}{\partial x_j} \left(\overline{u_j u_i} - \nu \frac{\partial U_i}{\partial x_j} \right)$$

Traditional Reynolds Stress

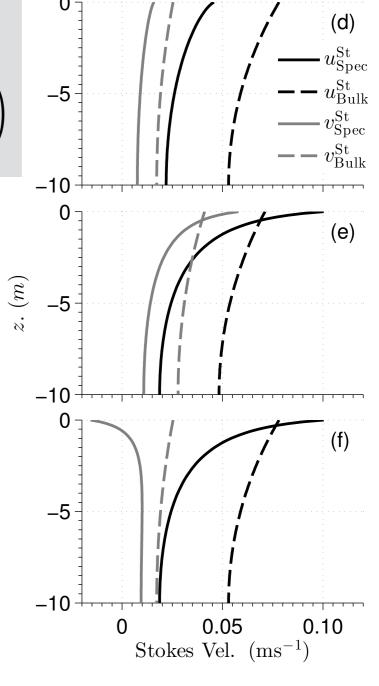
$$\overline{u'w'} = -K_M \frac{\partial U}{\partial z} \qquad \overline{v'w'} = -K_M \frac{\partial V}{\partial z}$$

$$K_M = c\sqrt{2kl}S_M$$

Reynolds Stress with C-L Vortex Force

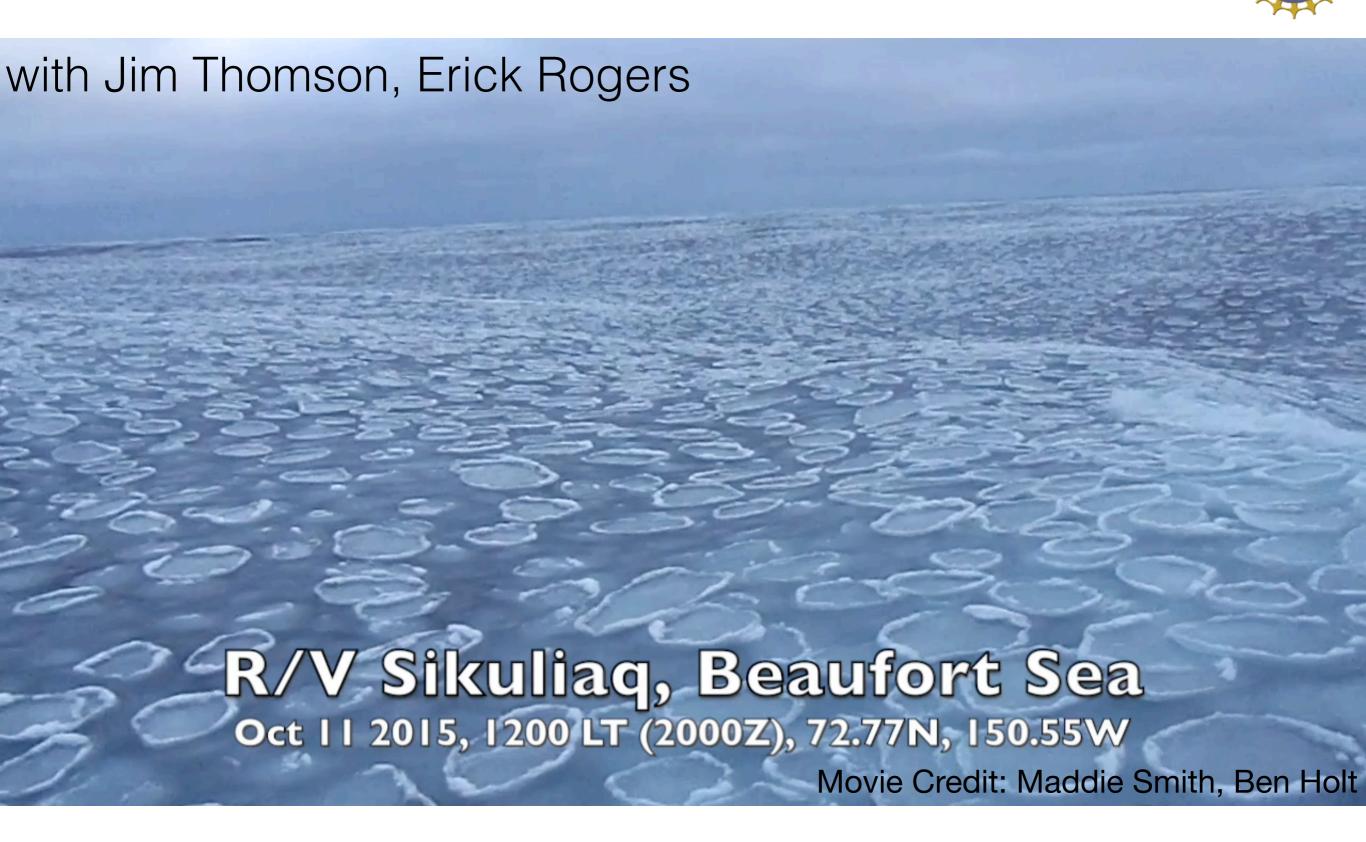
$$\overline{u'w'} = -K_M \frac{\partial U}{\partial z} - K_M^S \frac{\partial U^{\text{St}}}{\partial z} \qquad \overline{v'w'} = -K_M \frac{\partial V}{\partial z} - K_M^S \frac{\partial V^{\text{St}}}{\partial z}$$

$$K_M = c\sqrt{2kl}S_M \qquad K_M^S = c\sqrt{2kl}\frac{S_M^S}{S_M}$$



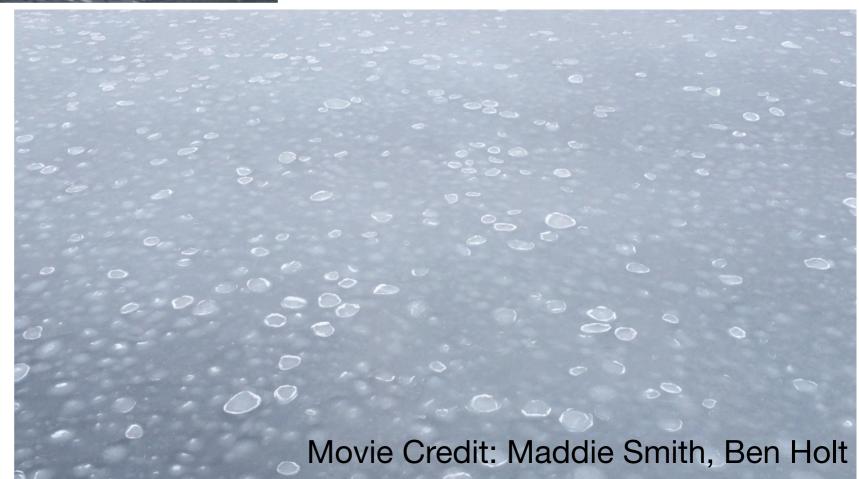
Harcourt, 2013, 2015 Zheng et al.,

Coastal Ocean Dynamics in the Arctic (CODA)

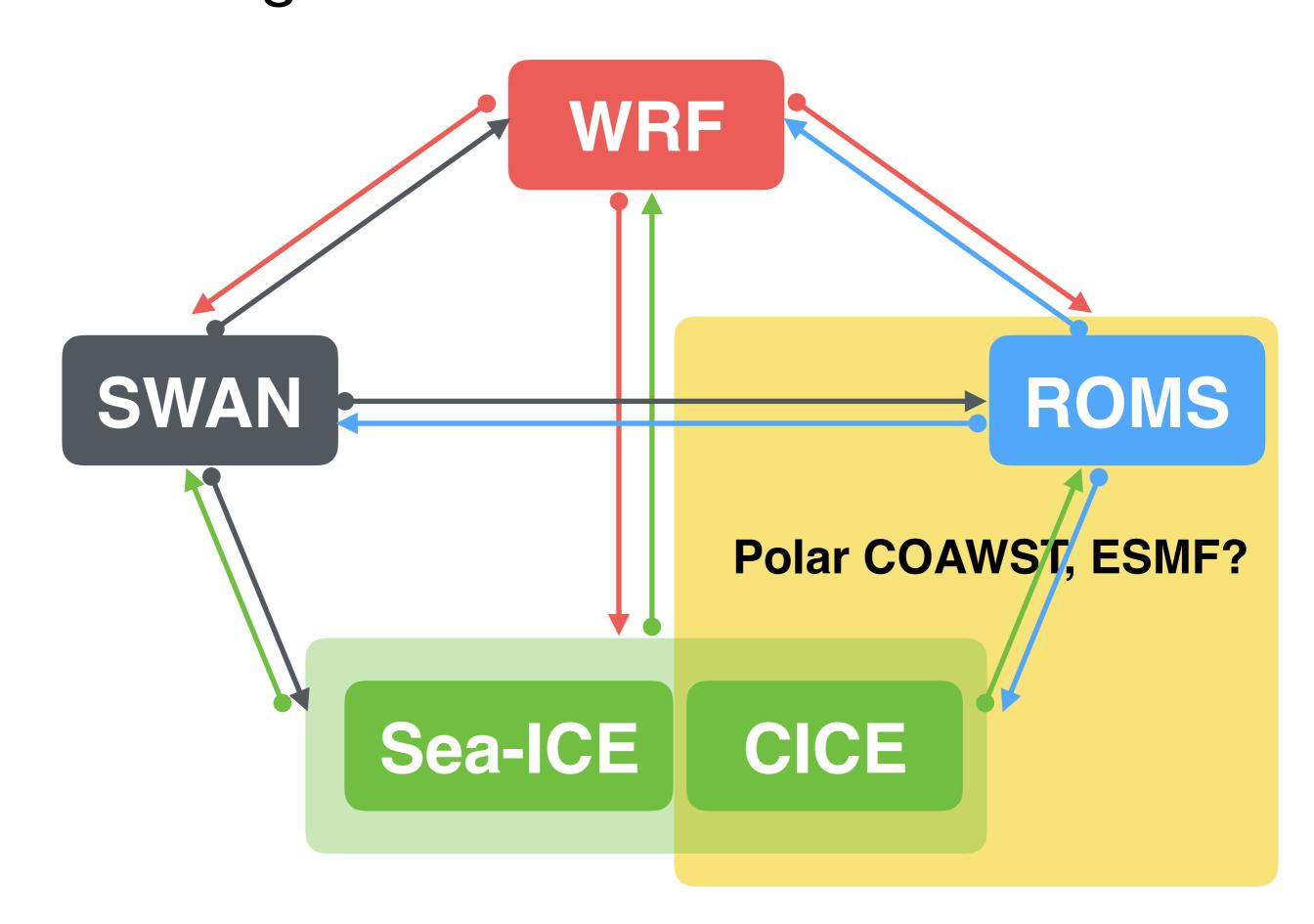


Wave-Ice Interaction





Modeling Wave-Ice Interaction- COAWST



SWAN with ICE

Action (N)-Balance Equation

$$\frac{\partial N}{\partial t} + \nabla \cdot \vec{c}N = \frac{S_{\text{tot}}}{\sigma}$$

$$\frac{\partial N}{\partial t} + \nabla \cdot \vec{c}N = \frac{1}{\sigma} \left(S_{\text{in}} + S_{\text{nl3}} + S_{\text{nl4}} + S_{\text{ds,w}} + S_{\text{ds,br}} \right)$$

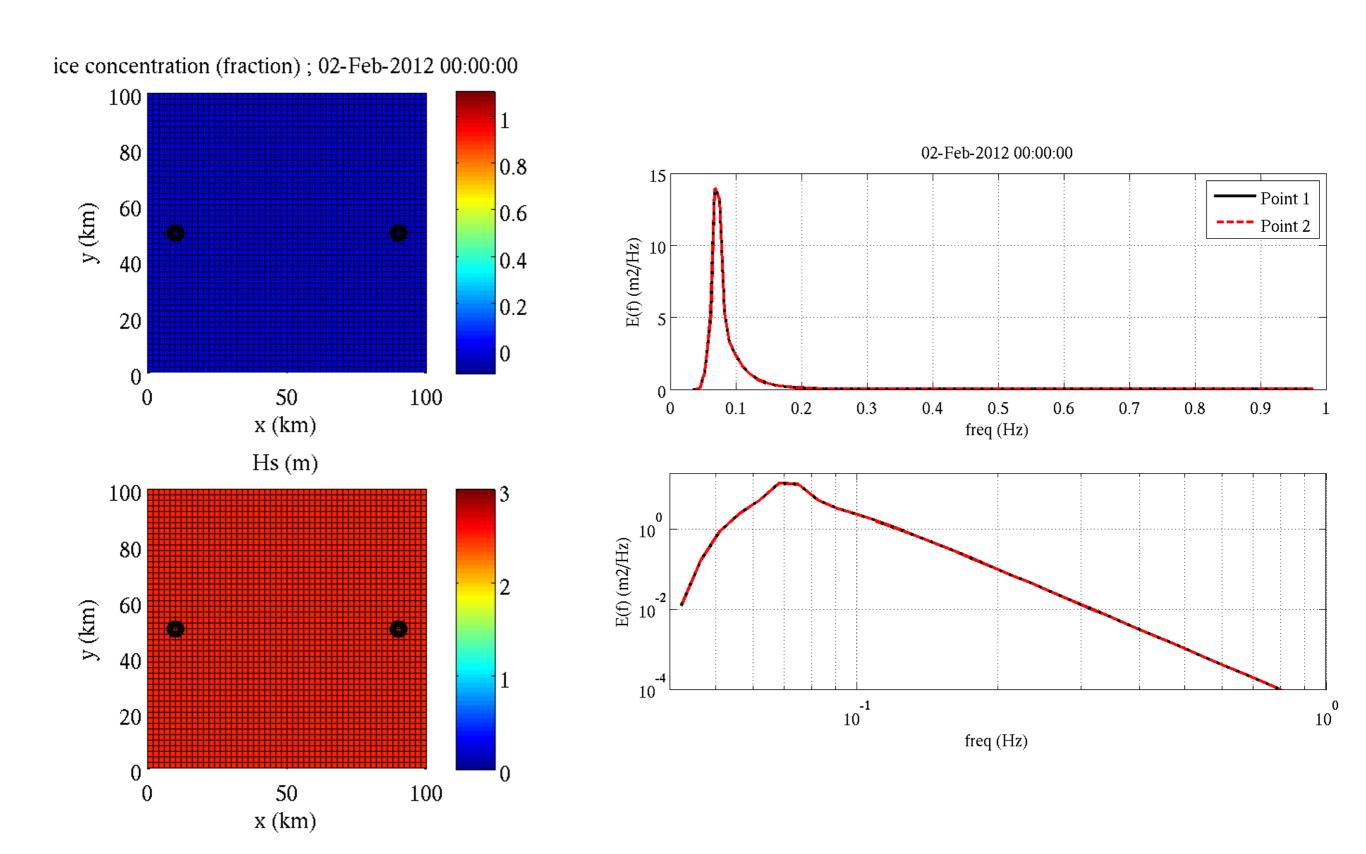
Action (N)-Balance Equation with ICE

$$\frac{\partial N}{\partial t} + \nabla \cdot \vec{c}N = \frac{1}{\sigma} \left(\frac{S_{\text{in}}(1 - \alpha)}{S_{\text{in}}(1 - \alpha)} + S_{\text{nl3}} + S_{\text{nl4}} + S_{\text{ds}} + \frac{S_{\text{ice}}}{S_{\text{ice}}} \right)$$

$$D_{\rm ice}=\frac{S_{\rm ice}}{E}=-C_g\alpha$$

$$\alpha = C_0+C_1f+C_2f^2+C_3f^3+C_4f^4$$
 Rogers et al., 2013

Idealized Examples



Rogers et al., 2019

Realistic Examples (Gulf of Bothnia)



